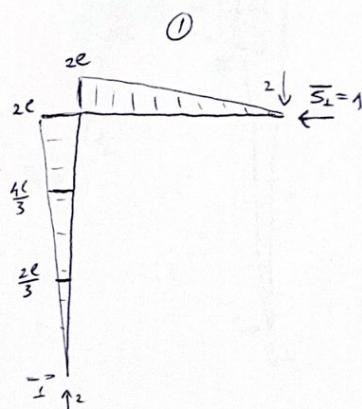
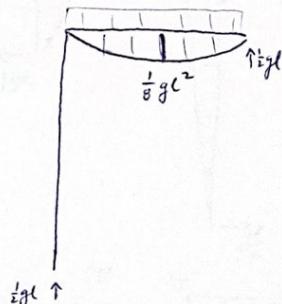
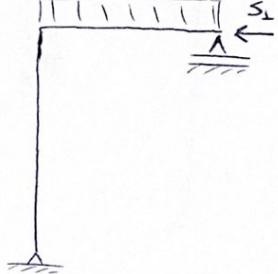
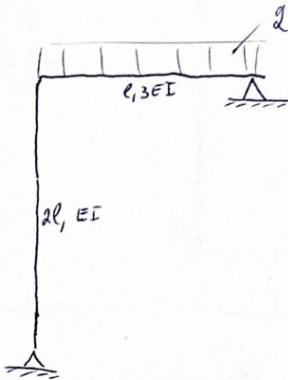


Zadanie - Verseczanie, statyczki nieadreduj.

- ① zadanie resiki transformacyjne osłonca B
o horizontalnym pokrewni osłonac



$$f_B = \alpha_1 s_1 + \Delta_1^2 = 0$$

$$\alpha_{11} = ① \times ① = \frac{1}{3EI} \left\{ \frac{1}{2} 2l \cdot l \cdot \frac{4l}{3} \right\} + \frac{1}{EI} \left\{ \frac{1}{2} 2l \cdot 2l \cdot \frac{4l}{3} \right\} = \frac{1}{EI} \left\{ \frac{4l^3}{9} + \frac{8l^3}{3} \right\} = \frac{28}{9} \frac{l^3}{EI}$$

$$\Delta_1^2 = ① \times ② = \frac{1}{3EI} \left\{ -2 \cdot \frac{2}{3} \frac{1}{8} gl^2 \frac{l}{2} \cdot l \right\} = -\frac{1}{36} \frac{gl^4}{EI}$$

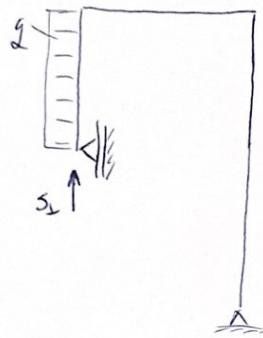
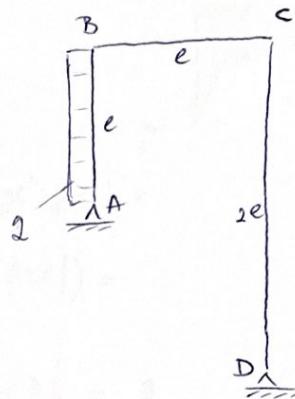
$$\frac{28}{9} \frac{gl^3}{EI} s_1 - \frac{1}{36} \frac{gl^4}{EI} = 0 \quad / \cdot 36$$

$$112 s_1 = gl$$

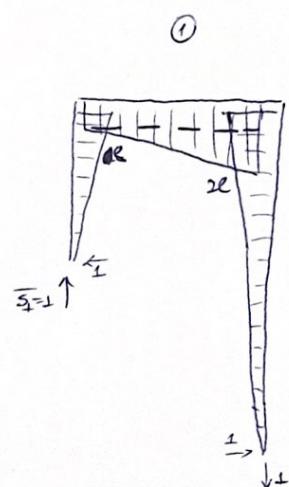
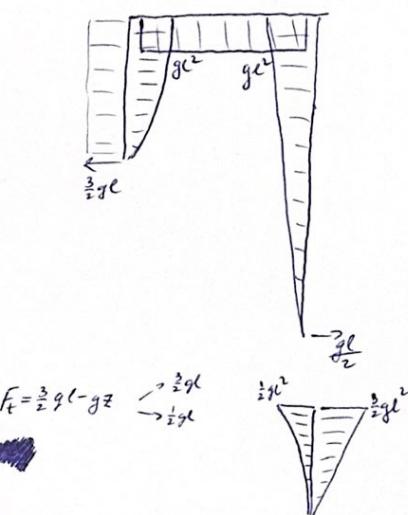
$$\boxed{s_1 = \frac{1}{112} gl}$$

② Řešit výšak statickě neodrážených veličin
horizontálnou pohybovací tukce C?

$$EI = \text{const.}$$



②



①

$$f_A^{net} = \alpha_{11} \cdot S_1 + \Delta_1^2 = 0$$

$$\alpha_{11} = \frac{1}{EI} \left\{ \frac{1}{2} gl \cdot l \cdot \frac{2}{3} l + c \cdot e - \frac{3}{2} e + \frac{1}{2} e \cdot e - \frac{5}{3} e + \frac{1}{2} 2e \cdot 2e \cdot \frac{4}{3} e \right\} = \frac{l^3}{EI} \left\{ \frac{1}{3} + \frac{2}{3} + \frac{5}{6} + \frac{8}{3} \right\} = \frac{16}{3} \frac{l^3}{EI}$$

$$\Delta_1^2 = \frac{1}{EI} \left\{ \frac{1}{2} gl^2 \cdot 2e \cdot \frac{4}{3} e + gl^2 \cdot e \cdot \frac{3}{2} e - \frac{1}{3} \frac{10}{2} gl^2 \cdot l \cdot \frac{3}{4} e + \frac{1}{2} \frac{3}{2} gl^2 \cdot e \cdot \frac{2}{3} e \right\} =$$

$$\Delta_1^2 = \frac{gl^4}{EI} \left\{ \frac{4}{3} + \frac{3}{2} - \frac{1}{8} + \frac{1}{2} \right\} = \frac{77}{24} \frac{gl^4}{EI}$$

$$\frac{16}{3} \frac{l^3}{EI} S_1 + 77 gl^4 = 0$$

$$\underline{\underline{S_1 = -\frac{77}{128} gl}}$$

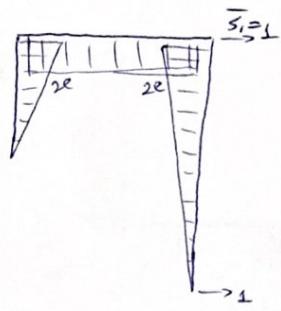
(2)

$$f_c^{\text{hor}} = \Delta_2^g + S_1 \cdot ① \cdot ②$$

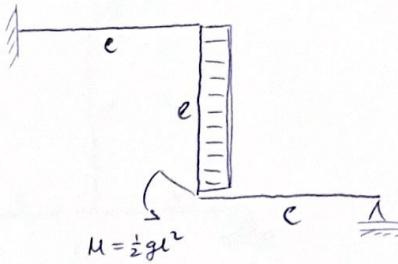
$$\begin{aligned} f_c^{\text{hor}} &= \frac{1}{EI} \left(\frac{1}{2} gl^2 \cdot 2e \cdot \frac{2}{3} 2e + gl^2 \cdot e \cdot 2e + \frac{1}{2} \frac{3}{2} gl^2 \cdot e \cdot \frac{2}{3} 2e - \frac{1}{3} \frac{1}{2} gl^2 \cdot \frac{3}{4} 2e \right) + \\ &+ S_1 \left(\frac{1}{EI} \left\{ \frac{1}{2} 2e \cdot 2e \cdot \frac{2}{3} 2e + \frac{e+2e}{2} e \cdot 2e + \frac{1}{2} e \cdot e \cdot \frac{2}{3} 2e \right\} \right) = \end{aligned}$$

$$f_c^{\text{hor}} = \frac{gl^4}{EI} \left\{ \frac{4}{3} + 2 + 1 - \frac{1}{4} \right\} - \frac{77}{128} \frac{gl^4}{EI} \left\{ \frac{8}{3} + 3 + \frac{2}{3} \right\} = 0$$

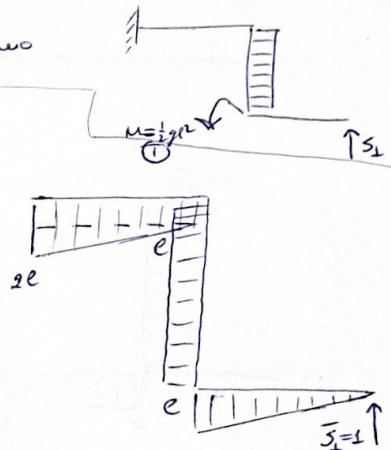
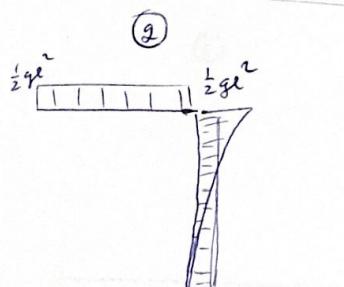
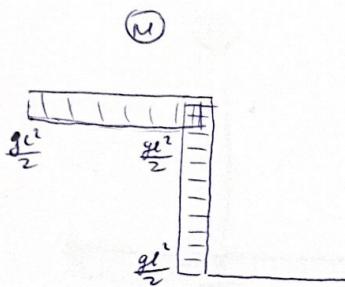
$$f_c^{\text{hor}} = \frac{gl^4}{EI} \left(\frac{49}{12} - \frac{77}{128} \cdot \frac{19}{3} \right) = \frac{105}{384} \frac{gl^4}{EI}$$



$$\textcircled{3} \quad EF = \text{const.}$$



proponka: kada iuvauo uklesteyje, da ga sauvauo



$$\int_{\delta}^{ret} = d_{11} S_1 + \Delta_1^M + \Delta_1^Q = 0$$

$$\alpha_{11} = \frac{1}{EI} \left\{ l \cdot l \cdot \frac{3}{2}e + \frac{1}{2}l \cdot e \cdot \left(e + \frac{2}{3}l\right) + l \cdot e \cdot e + \frac{1}{2}l \cdot e \cdot \frac{2}{3}l \right\} = \frac{l^3}{EI} \left(\frac{3}{2} + \frac{5}{6} + 1 + \frac{1}{3} \right) = \frac{11}{3} \frac{e^3}{EI}$$

$$\Delta_1^M = \frac{1}{EI} \left\{ \frac{1}{2} gl^2 \cdot e \cdot \frac{3}{2}e + \frac{1}{2} gl^2 \cdot e \cdot e \right\} = \frac{gl^4}{EI} \left(\frac{3}{2} + \frac{1}{2} \right) = \frac{5}{4} \frac{gl^4}{EI}$$

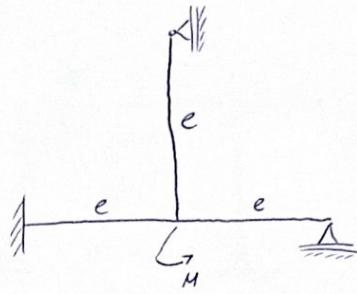
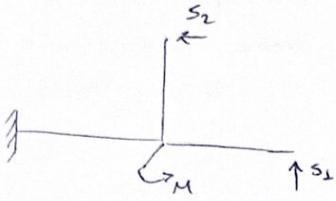
$$\Delta_{\perp}^2 = \frac{1}{EI} \left\{ -\frac{1}{2} gl^2 \cdot c \cdot \frac{3}{2}c - \frac{1}{3} \frac{1}{2} gl^2 \cdot c \cdot c \right\} = \frac{gl^4}{EI} \left(-\frac{3}{4} - \frac{1}{6} \right) = -\frac{11}{12} \frac{gl^4}{EI}$$

$$\frac{11}{3} \frac{E^3}{EI} \cdot S_1 + \frac{5}{4} \frac{gl^4}{EI} - \frac{11}{12} \frac{gl^4}{EI} = 0 \quad | \cdot \frac{3EI}{E^3}$$

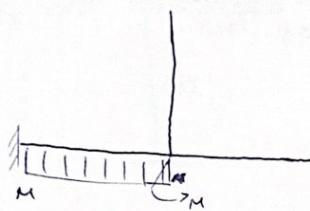
$$11 S_z + \frac{4}{4} g\ell = 0$$

$$S_z = -\frac{1}{11}ge$$

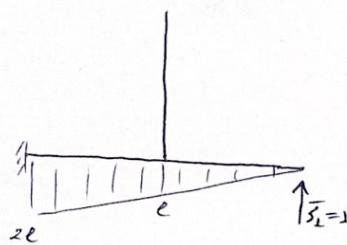
$$(4) EI = \text{const.}$$



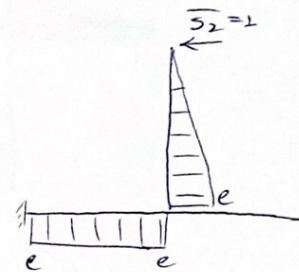
(R)



①



②



$$(1) f_B^{\text{vert}} = \alpha_{11} S_1 + \alpha_{21} S_2 + \Delta_1^M = 0$$

$$(2) f_B^{\text{hor}} = \alpha_{12} S_1 + \alpha_{22} S_2 + \Delta_2^M = 0$$

$$\alpha_{11} = \frac{1}{EI} \left\{ \frac{1}{2} e \cdot e \cdot \frac{2}{3} 2e \right\} = \frac{8}{3} \frac{e^3}{EI}$$

$$\alpha_{12} = \alpha_{21} = \frac{1}{EI} \left\{ \frac{2e+e}{2} e \cdot e \right\} = \frac{3}{2} \frac{e^3}{EI}$$

$$\Delta_1^M = \frac{1}{EI} \left\{ \frac{2e+e}{2} e \cdot M \right\} = \frac{3}{2} \frac{Me^2}{EI}$$

$$\Delta_2^M = \frac{1}{EI} \left\{ M \cdot e - e \right\} = \frac{Me^2}{EI}$$

$$(1) = 1 \frac{8}{3} \frac{e^3}{EI} S_1 + \frac{3}{2} \frac{e^3}{EI} S_2 + \frac{3}{2} \frac{Me^2}{EI} = 0 \quad | \cdot \frac{6EI}{e^2}$$

$$(2) = 1 \frac{3}{2} \frac{e^3}{EI} S_1 + \frac{4}{3} \frac{e^3}{EI} S_2 + \frac{Me^2}{EI} = 0 \quad | \cdot \frac{6EI}{e^2}$$

$$16S_1e + 9S_2e + 9M = 0$$

$$9S_1e + 8S_2e + 6M = 0$$

$$\Rightarrow S_1 = -\frac{9}{16}S_2 - \frac{9}{16}\frac{M}{e}$$

$$= 1 g \left(-\frac{9}{16}S_2 - \frac{9}{16}\frac{M}{e} \right) e + 8S_2e + 6M = 0$$

$$-\frac{81}{16}S_2e - \frac{81}{16}M + 8S_2e + 6M = 0$$

$$\frac{47}{16}S_2e + \frac{15}{16}M = 0 \Rightarrow S_2 = -\frac{15}{47}\frac{M}{e}$$

$$S_1 = -\frac{9}{16} \left(-\frac{15}{47}\frac{M}{e} \right) - \frac{9}{16}\frac{M}{e} = \left(\frac{135}{752} - \frac{423}{752} \right) \frac{M}{e}$$

$$S_2 = -\frac{288}{752}\frac{M}{e} = 1 S_2 = -\frac{18}{47}\frac{M}{e}$$

Писмени испит из ООК
Септембар - Октобар 2010.

- Статички неодређен равански носач промениле кругости оптерећен је континуалним оптерећењем дјактичким методом снага – Врешећијаков поступак израчунати статички непознате величине трансформацији носач у статички одређен на задати начин.
- Равански носач константне кругости EI оптерећен је силом F и моментом M према склопу.
Израчунати тражена параметра у функцији општих бројева.
- Израчунати максимални нормални напон у носачу користећи податке задате у склопу.
- Просторни носач константног кругног попречног пресека оптерећен је према склопу.
- Нацртати статичке дијаграме.
- Применом Хипотезе највећих напона симетрија опредити еквивалентни напон у увећашењу A у функцији F, a, W.
- Користећи податке из дјелатности у склопу које је дато доказати статички одређен носач.

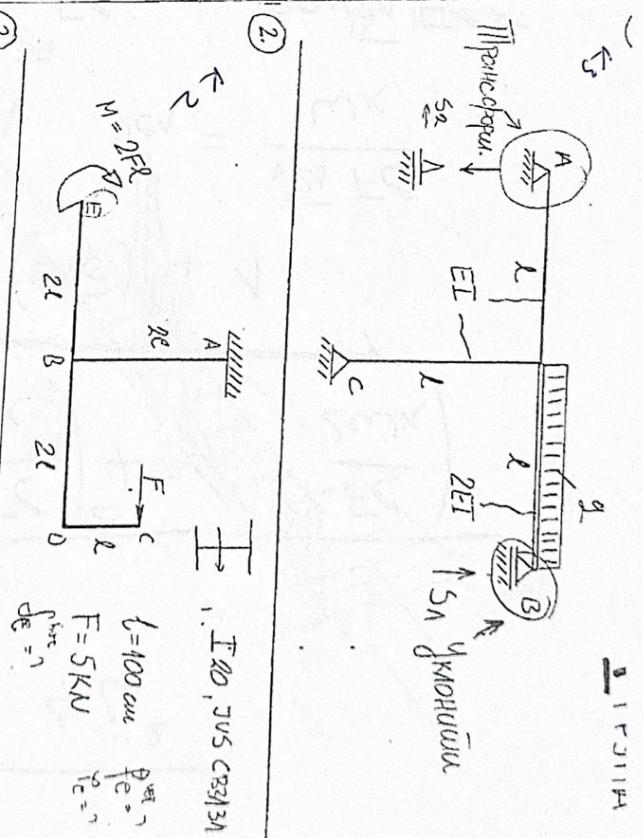
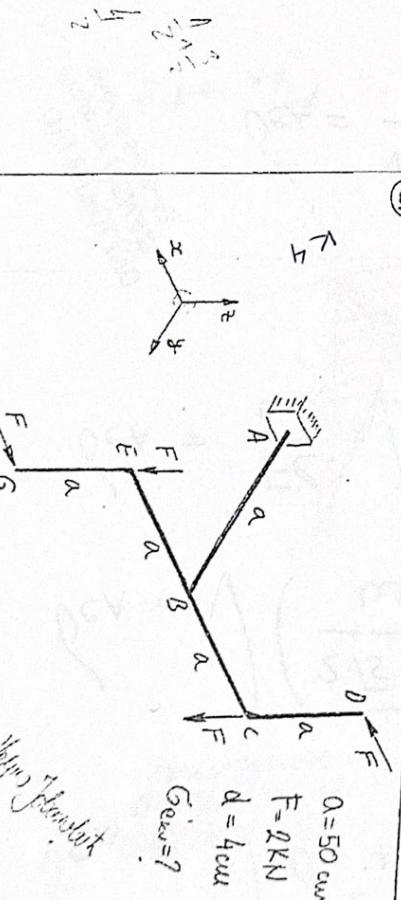
Напомене:

Испит траје три сата.

Дозвољено је само шtampana литература – не забораве!

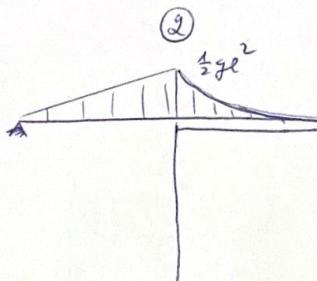
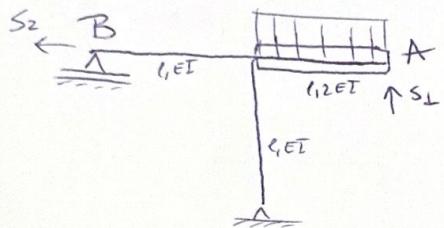
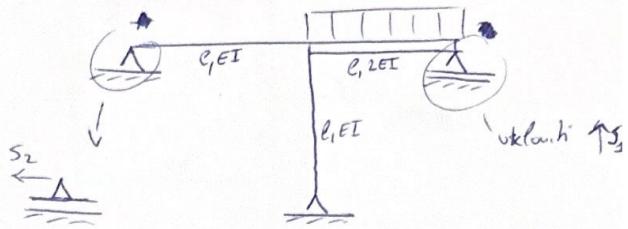
у Београду, 03.09.2010.

ČASOVI RAVOLJNO
Profesor NENAD
064/155-72-42

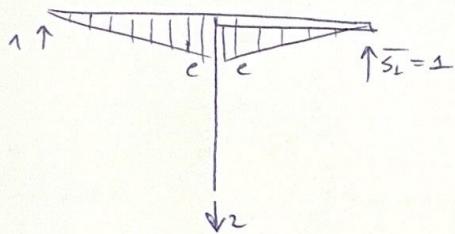


september 10

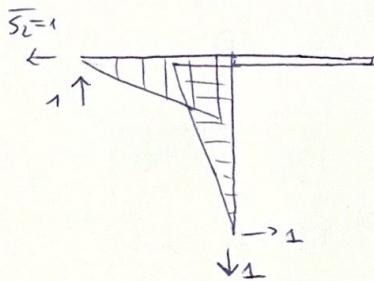
- ① izračunati nepoznate veličine transformišći uosac na zadati uocin



①



②



$$① f_A^{vert} = \alpha_{11} S_1 + \alpha_{12} S_2 + \Delta_1 = 0$$

$$② f_B^{hor} = \alpha_{21} S_1 + \alpha_{22} S_2 + \Delta_2 = 0$$

$$\alpha_{11} = \frac{1}{EI} \left\{ \frac{1}{2} e \cdot e \cdot \frac{2}{3} e \right\} + \frac{1}{2EI} \left\{ \frac{1}{2} e \cdot e \cdot \frac{2}{3} e \right\} = \frac{1}{2} \frac{e^3}{EI}$$

$$\alpha_{12} = \frac{1}{EI} \left\{ \frac{1}{2} e \cdot e \cdot \frac{2}{3} e \right\} = \frac{1}{3} \frac{e^3}{EI}$$

$$\alpha_{22} = \frac{1}{EI} \left\{ \frac{1}{2} e \cdot e \cdot \frac{2}{3} e \right\} = \frac{2}{3} \frac{e^3}{EI}$$

$$\Delta_1^1 = \frac{1}{EI} \left\{ -\frac{1}{2} \frac{1}{2} g e^2 \cdot e \cdot \frac{2}{3} e \right\} + \frac{1}{2EI} \left\{ -\frac{1}{3} \frac{1}{2} g e^2 \cdot e \cdot \frac{3}{4} e \right\} = -\frac{11}{48} \frac{g e^4}{EI}$$

$$\Delta_2^2 = \frac{1}{EI} \left\{ -\frac{1}{2} \frac{1}{2} g e^2 \cdot e \cdot \frac{2}{3} e \right\} = -\frac{1}{6} \frac{g e^4}{EI}$$

$$\frac{1}{2} \frac{e^3}{EI} S_1 + \frac{1}{3} \frac{e^3}{EI} S_2 - \frac{11}{48} \frac{g e^4}{EI} = 0 \quad | \cdot 2 \frac{EI}{C^3}$$

$$\frac{1}{3} \frac{e^3}{EI} S_1 + \frac{2}{3} \frac{e^3}{EI} S_2 - \frac{1}{6} \frac{g e^4}{EI} = 0 \quad | \cdot 3 \frac{EI}{C^3}$$

$$S_1 + \frac{2}{3} S_2 - \frac{11}{24} g e^2 = 0 \Rightarrow S_1 = \frac{11}{24} g e^2 - \frac{2}{3} S_2$$

$$\left(\frac{11}{24} g e^2 - \frac{2}{3} S_2 \right) + 2 S_2 - \frac{1}{2} g e^2 = 0$$

$$\frac{4}{3} S_2 - \frac{1}{24} g e^2 = 0 \Rightarrow S_2 = \frac{1}{32} \frac{g e^2}{EI}$$

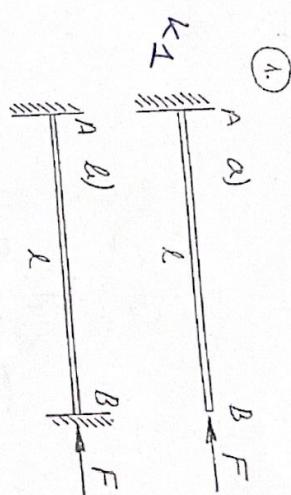
$$S_1 = \frac{11}{24} g e^2 - \frac{2}{3} \frac{1}{32} g e^2 = \frac{11}{24} g e^2 - \frac{1}{48} g e^2 =$$

$$= \boxed{S_1 = \frac{21}{48} g e^2}$$

109

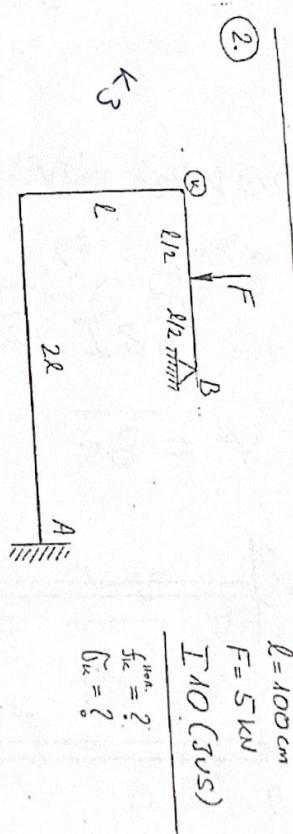
МАШИНСКИ ФАКУЛТЕТ УНИВЕРЗИТЕТА У БЕОГРАДУ
КАТЕДРА ЗА ОПТОРНОСТ КОНСТРУКЦИЈА

ПИСМЕНИ ИСТИГ из Основа опорности конструкција
(05.09.2009. год.)

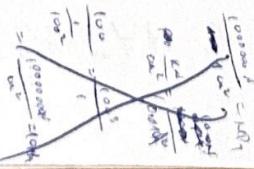


$$\begin{aligned}F_{ur} &=? \\c030 & \\I \text{ 16 (JUS)} & \\l = 100 \text{ cm} & \\E = 2,1 \cdot 10^4 \frac{\text{N}}{\text{cm}^2} &\end{aligned}$$

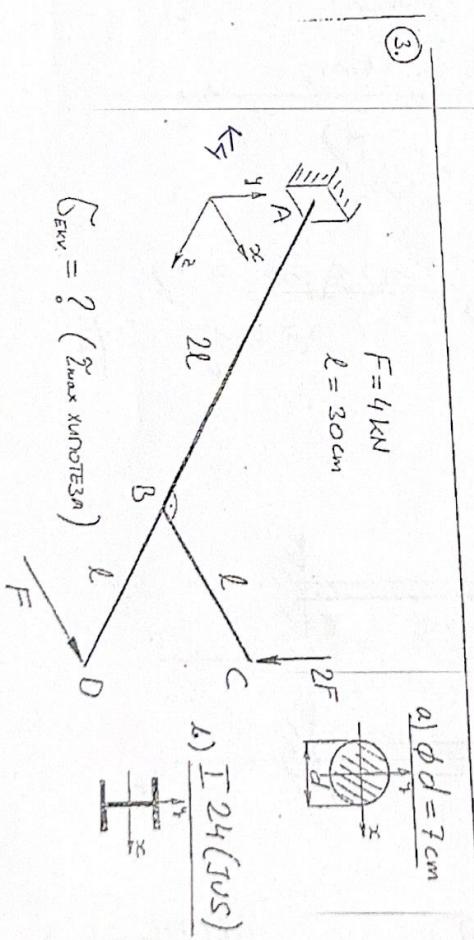
1. За приказане стањаје ослањаја челичног штапа, израчунати пренос критичне сниса испрљаја. Користити податке дате у склопу.
2. За конструирају приказашу на слици, користећи методу спајања Вертишанича поступак, усаглавати ослонац В израчунати стањемеконстанте величине и највећи дијаграм момената савијања у функцији од синих бројева. Користећи податке дате у склопу израчунати напон као и хоризонтално померавај преsek K.



$$\begin{aligned}l &= 100 \text{ cm} \\F &= 5 \text{ kN} \\I \text{ 10 (JUS)} & \\f_{ck}^{(tear)} &=? \\f_u &=?\end{aligned}$$



3. Челична конструкција залог појречног пресека оптерећена је према склопу. Користећи хипотезу максималних напона у конструкцији израчунати пренос критичнији скважиног напона у конструкцији ако је попречни пресек:
- a) кругли (d = 7 cm),
b) стандардни профил (I 24).
- Користите податке дате у склопу.



$$\begin{aligned}F &= 4 \text{ kN} \\l &= 30 \text{ cm} \\a) \quad \phi d &= 7 \text{ cm} \\I \text{ 24 (JUS)} &\end{aligned}$$

Напомене:

- Дозволета је употреба само шtamпane литејтуре.
- Максимум 3 сата.
- Резултати ће бити објављени у понедељак 07.09.2009. год.

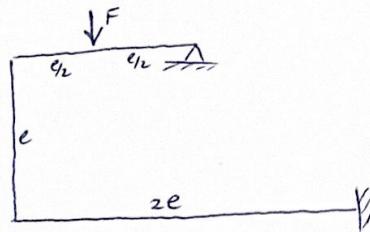
из Кабинета

Septembras 09

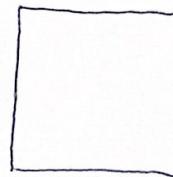
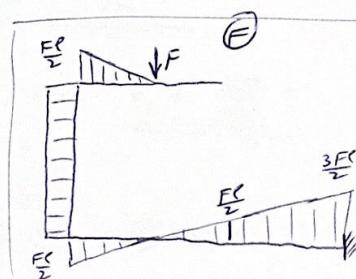
(2) uklaujaujame oslouca B

dijagramu wew. savijaciq?
(u opstuim Gopriima)

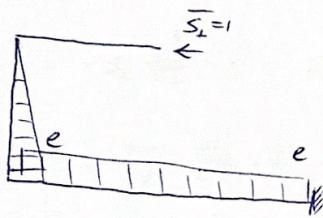
f_k^{hor} ? σ_k ?



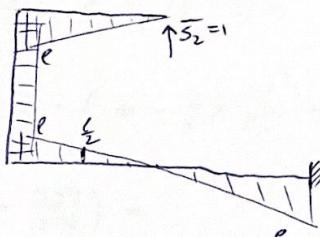
$$l = 100 \text{ cm}, \quad F = 5 \text{ kN}, \quad I = 10 \text{ (IUS)}$$



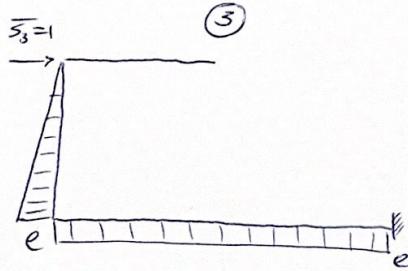
①



②



③



$$f_B^{\text{hor}} = d_{11} S_1 + d_{12} S_2 + \Delta_1^F = 0$$

$$f_B^{\text{vert}} = d_{21} S_1 + d_{22} S_2 + \Delta_2^F = 0$$

$$d_{11} = \frac{1}{EI} \left\{ \frac{1}{2} e \cdot e \cdot \frac{2}{3} e + e \cdot 2e \cdot e \right\} = \frac{7}{3} \frac{e^3}{EI}$$

$$d_{12} = d_{21} = \frac{1}{EI} \left\{ 0 + \frac{1}{2} e \cdot e \cdot e + 0 \right\} = \frac{1}{2} \frac{e^3}{EI}$$

$$d_{22} = \frac{1}{EI} \left\{ \frac{1}{2} e \cdot e \cdot \frac{2}{3} e + e \cdot e \cdot e + 2 \cdot \frac{1}{2} e \cdot e \cdot \frac{2}{3} e \right\} = 2 \frac{e^3}{EI}$$

$$\Delta_1^F = \frac{1}{EI} \left\{ -\frac{F^P}{2} \cdot e \cdot \frac{1}{2} e - \frac{1}{2} \frac{F^P}{2} \cdot \frac{1}{2} e + \frac{1}{2} \frac{3F^C}{2} \frac{3}{2} e \cdot e \right\} = \frac{FC^3}{EI} \left(-\frac{1}{4} - \frac{1}{8} + \frac{9}{8} \right) = \frac{3}{4} \frac{FC^3}{EI}$$

$$\begin{aligned} \Delta_2^F &= \frac{1}{EI} \left\{ -\frac{1}{2} \frac{F^P}{2} \frac{e}{2} \cdot \left(\frac{e}{2} + \frac{2}{3} \frac{e}{2} \right) - \frac{F^C}{2} e \cdot e - \frac{1}{2} \frac{F^C}{2} \cdot e \left(\frac{e}{2} + \frac{2}{3} \frac{e}{2} \right) + \frac{1}{2} \frac{F^C}{2} \cdot \frac{e}{2} \cdot \frac{1}{3} \frac{e}{2} - \frac{1}{2} e \cdot e \cdot \left(\frac{F^C}{2} + \frac{2}{3} F^C \right) \right\} = \\ &= \frac{FC^3}{EI} \left(-\frac{1}{8} \frac{5}{6} - \frac{1}{2} - \frac{1}{8} \frac{5}{6} + \frac{1}{48} - \frac{1}{2} \frac{7}{6} \right) = \frac{FC^3}{EI} \left(-\frac{5}{48} - \frac{24}{48} - \frac{5}{48} + \frac{1}{48} - \frac{28}{48} \right) = -\frac{61}{48} \frac{FC^3}{EI} \end{aligned}$$

$$\frac{7}{3} \frac{e^3}{EI} S_1 + \frac{1}{2} \frac{e^3}{EI} S_2 + \frac{3}{4} \frac{Fc^3}{EI} = 0 \quad | \cdot 2 \frac{EI}{e^3}$$

$$\frac{1}{2} \frac{e^3}{EI} S_1 + 2 \frac{e^3}{EI} S_2 - \frac{61}{48} \frac{Fc^3}{EI} = 0 \quad | \cdot \frac{EI}{e^3}$$

$$\frac{14}{3} S_1 + S_2 + \frac{3}{2} F = 0 \quad \Rightarrow \quad S_2 = -\frac{14}{3} S_1 - \frac{3}{2} F$$

$$\frac{1}{2} S_1 + 2 \left(-\frac{14}{3} S_1 - \frac{3}{2} F \right) - \frac{61}{48} F = 0$$

$$\frac{1}{2} S_1 - \frac{205}{3} S_1 - 3F - \frac{61}{48} F = 0$$

$$-\frac{53}{6} S_1 - \frac{205}{48} F = 0$$

$$S_1 = -\frac{205 \cdot 6}{48 \cdot 53} F \quad \Rightarrow \quad \underline{\underline{S_1 = -\frac{205}{424} F}}$$

$$S_2 = +\frac{14}{3} \frac{205}{424} F - \frac{3}{2} F \quad \Rightarrow \quad \underline{\underline{S_2 = \frac{481}{636} F}}$$

$$f_k^{hor} = \underbrace{S_1 \cdot ① \cdot ③}_{(④ \cdot ③)} + \underbrace{S_2 \cdot ② \cdot ③}_{(⑤ \cdot ③)} + \underbrace{(F) \cdot ③}_{(⑥ \cdot ③)} =$$

$$f_k^{hor} = S_1 \frac{1}{EI} \left\{ -\frac{1}{2} e \cdot e \cdot \frac{1}{3} e - e \cdot 2e \cdot e \right\} + S_2 \cdot \frac{1}{EI} \left\{ 0 + e \cdot e \cdot \frac{1}{2} e + 0 \right\} + \frac{1}{EI} \left(\frac{Ee}{2} \cdot e \cdot \frac{1}{2} e + \dots - e \cdot e \cdot \left(\frac{Ee}{2} + \frac{Ee}{2} \right) \right) =$$

$$f_k^{hor} = -S_1 \frac{e^3}{EI} \cdot \frac{1}{3} - S_2 \cdot \frac{e^3}{EI} \cdot \frac{1}{2} + F \cdot \frac{e^3}{EI} \left(\frac{1}{4} - 1 \right) =$$

$$f_k^{hor} = + \frac{205}{424} \frac{Fc^3}{EI} \cdot \frac{1}{3} - \frac{481}{636} \frac{Fc^3}{EI} \cdot \frac{1}{2} - \frac{3}{4} F \frac{Fc^3}{EI} =$$

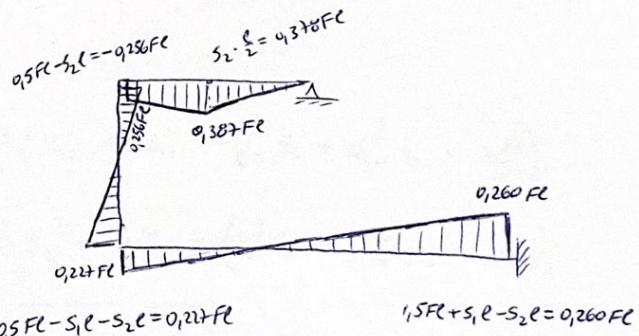
$$f_k^{hor} = \frac{Fc^3}{EI} \left(\frac{1435}{1272} - \frac{481}{1272} - \frac{954}{1272} \right) =$$

$$\underline{\underline{f_k^{hor} = 0}}$$

$$W_x = 34,2 \text{ cm}^3 \quad - \quad \text{za I10 (Aus)}$$

$$C_k = \frac{M_k}{W_x} = \frac{0,256 F}{34,2} = \frac{0,256 \cdot 5 \cdot 100}{34,2} =$$

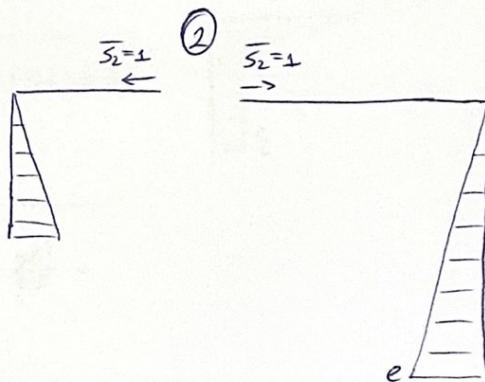
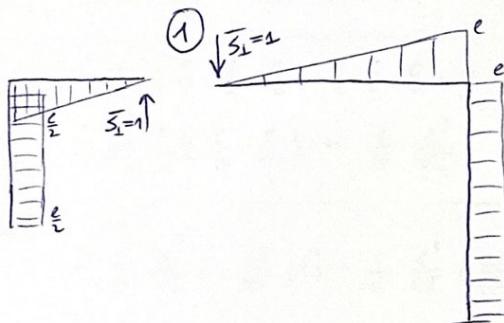
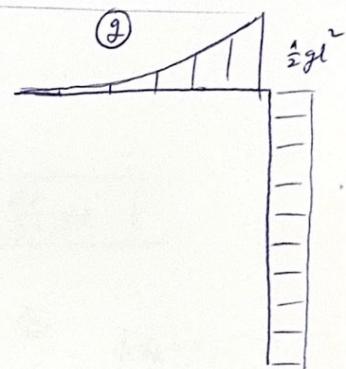
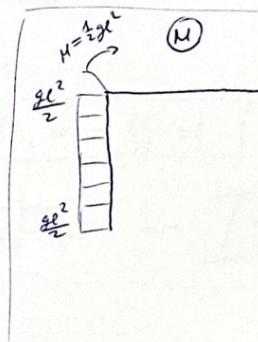
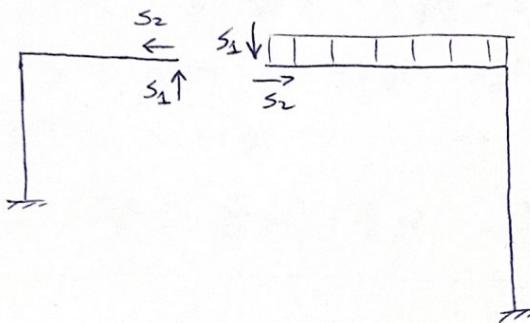
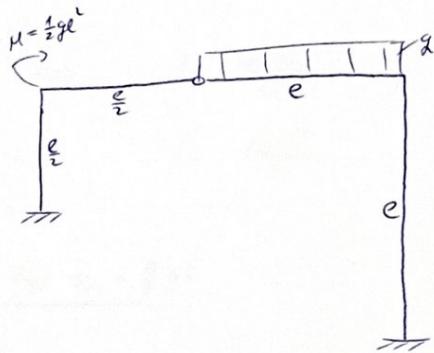
$$\underline{\underline{C_k = 3,74 \frac{kN}{cm^2}}}$$



(5) stat. ucp. reaktion?

$$f_{G, \text{stat}} = ?$$

Diagramm was. savigajia?



$$(1) f_{G, \text{rec}}^{\text{vert}} = \alpha_{11} S_1 + \alpha_{12} S_2 + \Delta_1^M + \Delta_1^2 = 0$$

$$(2) f_{G, \text{rec}}^{\text{hor}} = \alpha_{21} S_1 + \alpha_{22} S_2 + \Delta_2^M + \Delta_2^2 = 0$$

$$\alpha_{11} = \frac{1}{EI} \left\{ \frac{1}{2} \frac{e}{2} \frac{e}{2} \cdot \frac{2}{3} \frac{e}{2} + \frac{e}{2} \frac{e}{2} \frac{e}{2} + \frac{1}{2} e \cdot e \cdot \frac{2}{3} e + e \cdot e \cdot e \right\} = \frac{e^3}{EI} \left(\frac{1}{24} + \frac{1}{6} + \frac{1}{3} + 1 \right) = \frac{3}{2} \frac{e^3}{EI}$$

$$\alpha_{12} = \frac{1}{EI} \left\{ \frac{e}{2} \cdot \frac{e}{2} \cdot \frac{e}{4} - e \cdot e \cdot \frac{e}{2} \right\} = \frac{e^3}{EI} \left(\frac{1}{16} - \frac{1}{2} \right) = -\frac{7}{16} \frac{e^3}{EI}$$

$$\alpha_{22} = \frac{1}{EI} \left\{ \frac{1}{2} \frac{e}{2} \frac{e}{2} \cdot \frac{2}{3} \frac{e}{2} + \frac{1}{2} e \cdot e \cdot \frac{2}{3} e \right\} = \frac{e^3}{EI} \left(\frac{1}{24} + \frac{1}{3} \right) = \frac{3}{8} \frac{e^3}{EI}$$

$$\Delta_1^M = \frac{1}{EI} \left\{ -\frac{ge^2}{2} \cdot \frac{e}{2} \cdot \frac{e}{2} \right\} = -\frac{1}{8} \frac{ge^4}{EI}$$

$$\Delta_1^2 = \frac{1}{EI} \left\{ \frac{1}{3} \frac{ge^2}{EI} e \cdot \frac{3}{4} e + \frac{ge^2}{2} \cdot e \cdot e \right\} = \frac{5}{8} \frac{ge^4}{EI}$$

$$\Delta_2^M = \frac{1}{EI} \left\{ -\frac{ge^2}{2} \cdot \frac{e}{2} \cdot \frac{e}{4} \right\} = -\frac{1}{16} \frac{ge^4}{EI}$$

$$\Delta_2^2 = \frac{1}{EI} \left\{ -\frac{ge^2}{2} \cdot e \cdot \frac{e}{2} \right\} = -\frac{1}{4} \frac{ge^4}{EI}$$

$$\frac{3}{2} \frac{e^3}{EI} s_1 - \frac{7}{16} \frac{e^3}{EI} s_2 - \frac{1}{8} \frac{gl^4}{EI} + \frac{5}{8} \frac{gl^4}{EI} = 0 \quad / \cdot \frac{16EI}{e^3}$$

$$-\frac{7}{16} \frac{e^3}{EI} s_1 + \frac{3}{8} \frac{e^3}{EI} s_2 - \frac{1}{16} \frac{gl^4}{EI} - \frac{1}{4} \frac{gl^4}{EI} = 0 \quad / \cdot \frac{16EI}{e^3}$$

$$24 s_1 - 7 s_2 + 8 gl = 0 \Rightarrow s_2 = \frac{24}{7} s_1 + \frac{8}{7} gl$$

$$-7 s_1 + 6 s_2 - 5 gl = 0$$

$$-7 s_1 + 6 \left(\frac{24}{7} s_1 + \frac{8}{7} gl \right) - 5 gl = 0 \quad | \cdot 7$$

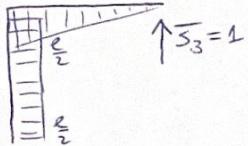
$$-49 s_1 + 144 s_1 + 48 gl - 35 gl = 0$$

$$95 s_1 + 13 gl = 0 \Rightarrow s_1 = -\frac{13}{95} gl$$

$$s_2 = \frac{24}{7} \left(-\frac{13}{95} gl \right) + \frac{8}{7} gl = -\frac{312 + 760}{7 \cdot 95} gl \Rightarrow s_2 = \frac{64}{95} gl$$

$$f_g^{vert} = \alpha_{31} s_1 + \alpha_{32} s_2 + \Delta_3^M + \Delta_3^Q$$

(3)



$$\alpha_{31} = \frac{1}{EI} \left\{ \frac{e}{2} \cdot \frac{e}{2} \cdot \frac{e}{2} + \frac{1}{2} \frac{e}{2} \cdot \frac{e}{2} \cdot \frac{2}{3} \frac{e}{2} \right\} = \frac{e^3}{EI} \left(\frac{1}{8} + \frac{1}{24} \right) = \frac{1}{6} \frac{e^3}{EI}$$

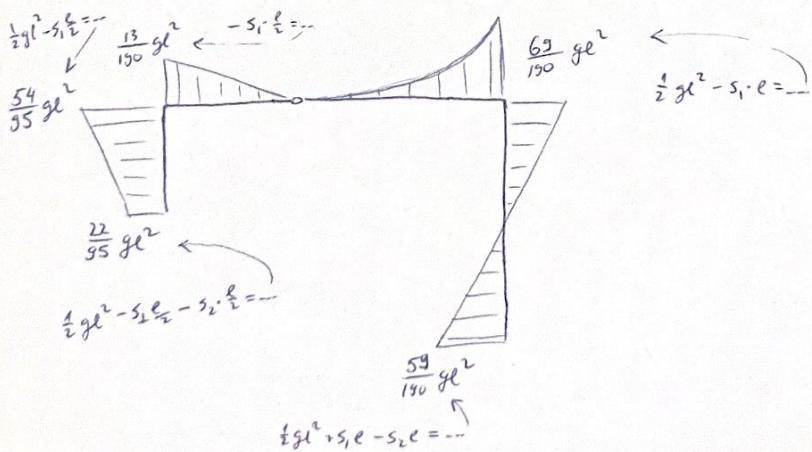
$$\alpha_{32} = \frac{1}{EI} \left\{ \frac{e}{2} \frac{e}{2} \cdot \frac{e}{4} \right\} = \frac{1}{16} \frac{e^3}{EI}$$

$$f_g^{vert} = \frac{1}{6} \frac{e^3}{EI} \left(-\frac{13}{95} gl \right) + \frac{1}{16} \frac{e^3}{EI} \left(\frac{64}{95} gl \right) - \frac{1}{8} \frac{gl^4}{EI} =$$

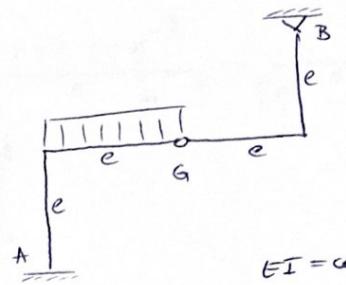
$$f_g^{vert} = \frac{gl^4}{EI} \left(-\frac{13}{570} + \frac{24}{570} - \frac{285}{2280} \right) =$$

$$f_g^{vert} = -\frac{241}{2280} \frac{gl^4}{EI}$$

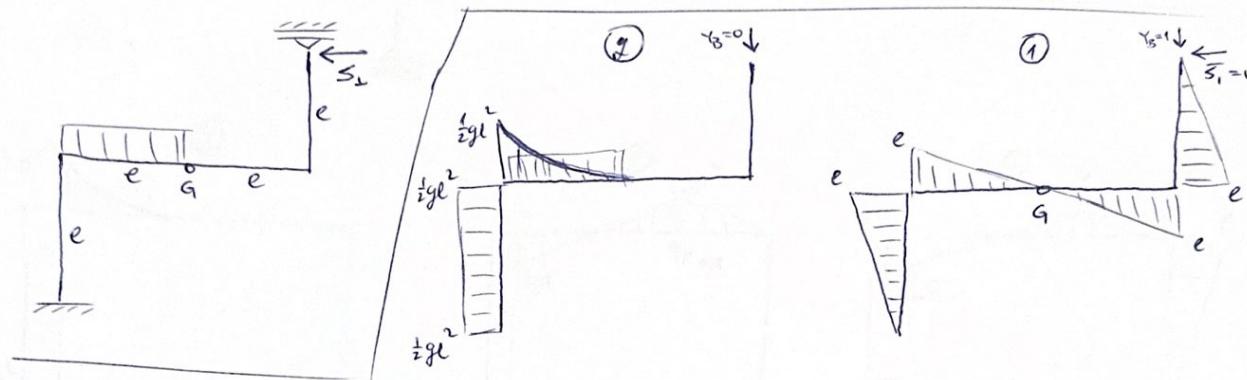
ZGMI diagramm won. scv: (1) + (2) + s₁ · (1) + s₂ · (2)



⑥ načrtati zbirni dijagram momenata sileksije



$$EI = \text{const.}$$



$$\Delta_{11} + S_1 + \Delta_1^2 = 0$$

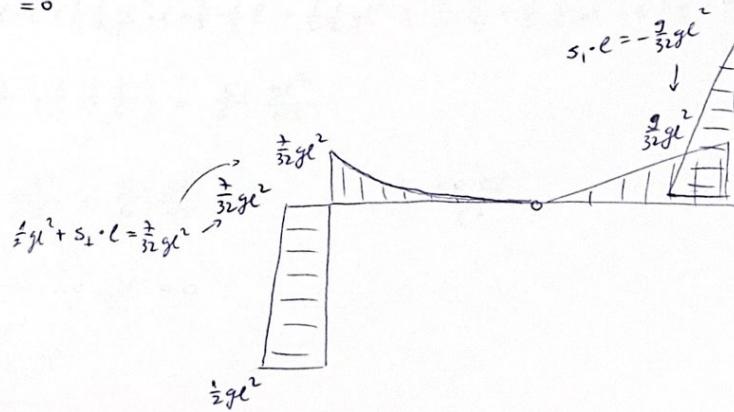
$$\Delta_{11} = \frac{1}{EI} \left\{ \frac{1}{2} l \cdot l \cdot \frac{2}{3} e \right\} \cdot 4 = \frac{4}{3} \frac{l^3}{EI}$$

$$\Delta_1^2 = \frac{1}{EI} \left\{ \frac{1}{2} gl^2 \cdot l \cdot \frac{l}{2} + \frac{1}{3} \frac{1}{2} gl^2 \cdot e \cdot \frac{3}{4} e \right\} = \frac{gl^4}{EI} \left(\frac{1}{4} + \frac{1}{8} \right) = \frac{3}{8} \frac{gl^4}{EI}$$

$$\frac{4}{3} \frac{l^3}{EI} S_1 + \frac{3}{8} \frac{gl^4}{EI} = 0 \quad / \cdot \frac{24EI}{l^3}$$

$$32 S_1 + 9 gl = 0$$

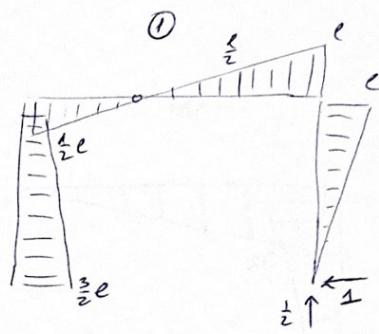
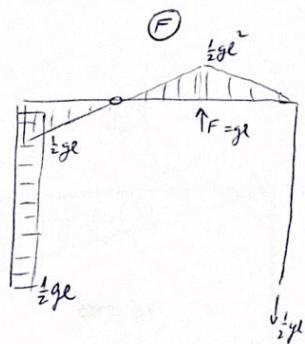
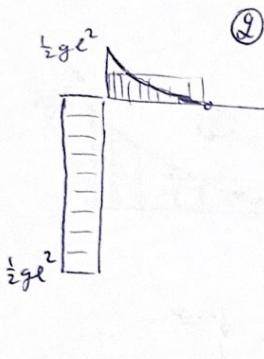
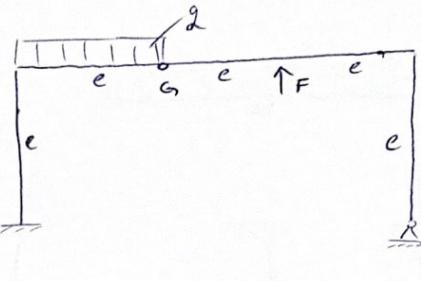
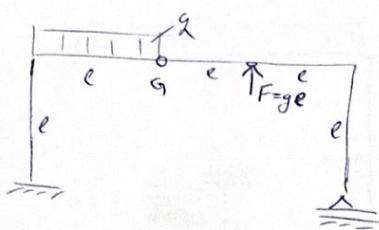
$$\underline{S_1 = -\frac{9}{32} gl}$$



(7)

$$F = gl$$

$$EI = \text{const.}$$



$$\alpha_u S_1 + \Delta_1^S + \Delta_1^F = 0$$

$$\alpha_u = \frac{1}{EI} \left\{ \frac{1}{2} l \cdot l \cdot l + \frac{1}{2} l \cdot l \cdot \left(\frac{1}{2} l + \frac{2}{3} l \right) + \frac{1}{2} \frac{1}{2} l \cdot l \cdot \frac{2}{3} \frac{1}{2} l + \frac{1}{2} l \cdot 2l \cdot \frac{2}{3} l + \frac{1}{2} l \cdot l \cdot \frac{2}{3} l \right\} =$$

$$\alpha_u = \frac{l^3}{EI} \left(\frac{1}{3} + \frac{1}{12} + \frac{2}{3} + \frac{1}{2} + \frac{7}{12} \right) = \frac{13}{6} \frac{l^3}{EI}$$

$$\Delta_1^S = \frac{1}{EI} \left\{ -\frac{1}{2} gl^2 \cdot l \cdot l - \frac{1}{3} \frac{1}{2} gl^2 \cdot l \cdot \frac{3}{4} \frac{1}{2} l \right\} = \frac{gl^4}{EI} \left\{ -\frac{1}{2} - \frac{1}{16} \right\} = -\frac{9}{16} \frac{gl^4}{EI}$$

$$\Delta_1^F = \frac{1}{EI} \left\{ \frac{1}{2} gl^2 \cdot l \cdot l + \frac{1}{2} \frac{1}{2} gl^2 \cdot l \cdot \frac{2}{3} - \frac{1}{2} l + \frac{1}{2} \frac{1}{2} gl^2 \cdot l \cdot \frac{2}{3} \frac{1}{2} + \frac{1}{2} \frac{1}{2} gl^2 \cdot l \left(\frac{1}{2} + \frac{2}{3} \frac{1}{2} \right) \right\} =$$

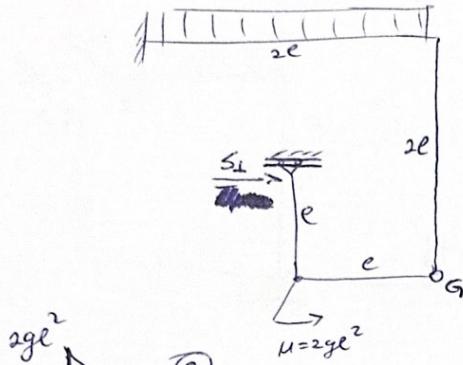
$$\Delta_1^F = \frac{gl^4}{EI} \left\{ \frac{1}{2} + \frac{1}{12} + \frac{1}{12} + \frac{1}{6} \right\} = \frac{5}{6} \frac{gl^4}{EI}$$

$$\frac{13}{6} \frac{l^3}{EI} S_1 - \frac{9}{16} \frac{gl^4}{EI} + \frac{5}{6} \frac{gl^4}{EI} = 0 \quad / \circ \frac{48 EI}{l^3}$$

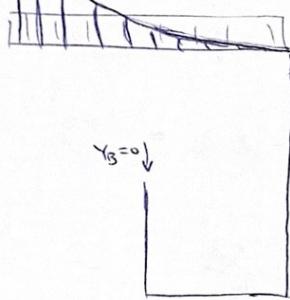
$$104 S_1 - 27 gl + 40 gl = 0$$

$$\underline{\underline{S_1 = -\frac{13}{104} gl = -\frac{1}{8} gl}}$$

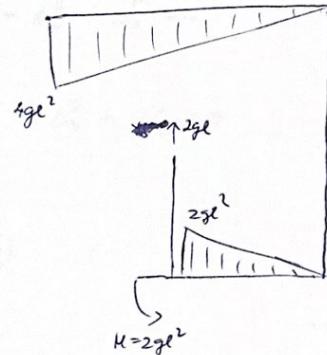
⑧ $EI = \text{const.}$



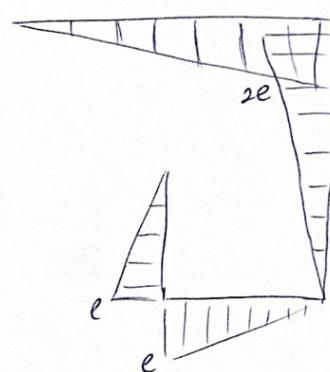
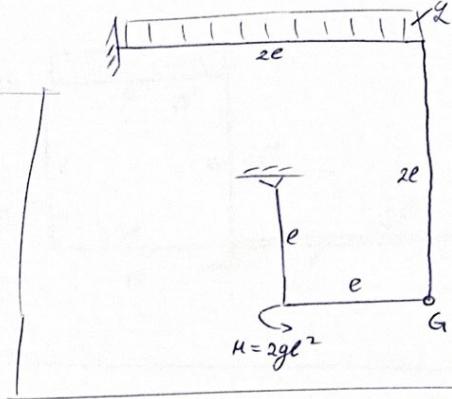
$$2ge^2$$



$$\gamma_B = 0$$



$$K = 2ge^2$$



$$\Delta_{11} S_L + \Delta_{12} + \Delta_{13} = 0$$

$$\Delta_{11} = \frac{1}{EI} \left\{ \frac{1}{2} e \cdot e \cdot \frac{2}{3} e + \frac{1}{2} e \cdot e \cdot \frac{2}{3} e + \frac{1}{2} 2e \cdot 2e - \frac{2}{3} 2e \right\} = \frac{e^3}{EI} \left(\frac{1}{3} + \frac{1}{3} + \frac{8}{3} + \frac{8}{3} \right) = 6 \frac{e^3}{EI}$$

$$\Delta_{12} = \frac{1}{EI} \left\{ -\frac{1}{3} 2ge^2 \cdot 2e \cdot \frac{1}{4} 2e \right\} = -\frac{2}{3} \frac{ge^4}{EI}$$

$$\Delta_{13} = \frac{1}{EI} \left\{ \frac{1}{2} 4ge^2 \cdot 2e \cdot \frac{1}{3} 2e \right\} - \frac{1}{2} 2ge^2 \cdot e \cdot \frac{2}{3} e = \frac{2e^4}{EI} \left(\frac{8}{3} - \frac{2}{3} \right) = 2 \frac{ge^4}{EI}$$

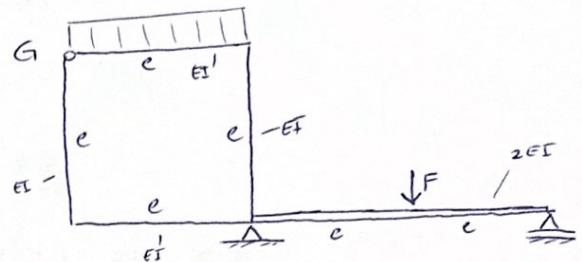
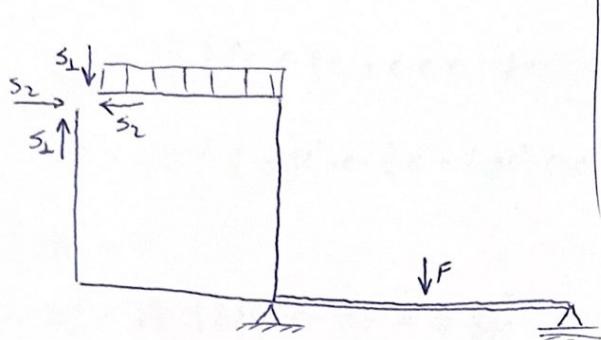
$$6 \frac{e^3}{EI} \cdot S_L - \frac{2}{3} \frac{ge^4}{EI} + 2 \frac{ge^4}{EI} = 0 \quad / \cdot 3 \frac{EI}{e^3}$$

$$18 S_L - 2ge + 6ge = 0$$

$$18 S_L + 4ge = 0$$

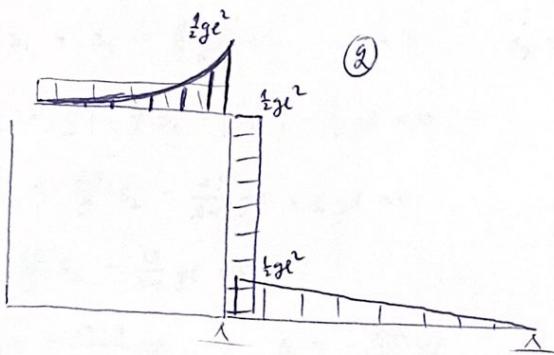
$$\underline{\underline{S_L = -\frac{2}{9} ge}}$$

(9.)



$$(1) f_{G,\text{ret}}^{\text{rel}} = \alpha_{11} S_1 + \alpha_{12} S_2 + \Delta_1^F + \Delta_2^F = 0$$

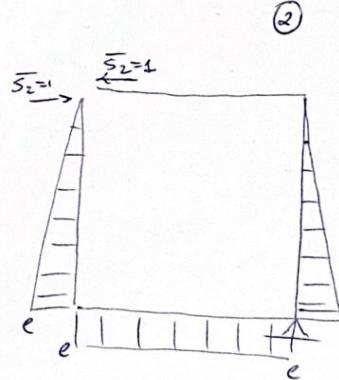
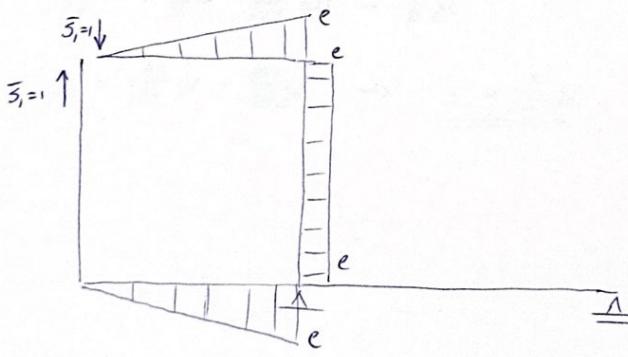
$$(2) f_{G,\text{hor}}^{\text{rel}} = \alpha_{21} S_1 + \alpha_{22} S_2 + \Delta_1^F + \Delta_2^F = 0$$



(g)

(F)

(1)



(2)

$$\alpha_{11} = \frac{1}{EI} \left\{ \frac{1}{2} l \cdot l \cdot \frac{2}{3} l + c \cdot e \cdot e + \frac{1}{2} l \cdot e \cdot \frac{2}{3} l \right\} = \frac{5}{3} \frac{l^3}{EI}$$

$$\alpha_{12} = \frac{1}{EI} \left\{ e \cdot e \cdot \frac{l}{2} + e \cdot e \cdot \frac{l}{2} \right\} = \frac{l^3}{EI}$$

$$\alpha_{22} = \frac{1}{EI} \left\{ \frac{1}{2} l \cdot l \cdot \frac{2}{3} l + e \cdot e \cdot e + \frac{1}{2} l \cdot e \cdot e \cdot \frac{2}{3} l \right\} = \frac{5}{3} \frac{l^3}{EI}$$

$$\Delta_1^Q = \frac{1}{EI} \left\{ \frac{1}{3} \frac{1}{2} g e^2 \cdot e \cdot \frac{3}{4} l + \frac{1}{2} g e^2 \cdot e \cdot e \right\} = \frac{g l^4}{EI} \left(\frac{1}{8} + \frac{1}{2} \right) = \frac{5}{8} \frac{g l^4}{EI}$$

$$\Delta_1^F = 0$$

$$\Delta_2^Q = \frac{1}{EI} \left\{ \frac{1}{2} g e^2 \cdot e \cdot \frac{l}{2} \right\} = \frac{1}{4} \frac{g l^4}{EI}$$

$$\Delta_2^F = 0$$

$$\frac{5}{3} \frac{l^3}{EI} s_1 + \frac{l^3}{EI} s_2 + \frac{5}{8} \frac{g l^4}{EI} = 0 \quad | \cdot \frac{EI}{l^3}$$

$$\frac{l^3}{EI} s_1 + \frac{5}{3} \frac{l^3}{EI} s_2 + \frac{1}{4} \frac{g l^4}{EI} = 0 \quad | \cdot \frac{EI}{l^3}$$

$$\frac{5}{3} s_1 + s_2 + \frac{5}{8} g l = 0 \quad \Rightarrow \quad s_2 = -\frac{5}{3} s_1 - \frac{5}{8} g l$$

$$s_1 + \frac{5}{3} \left(-\frac{5}{3} s_1 - \frac{5}{8} g l \right) + \frac{1}{4} g l = 0$$

$$s_1 - \frac{25}{9} s_1 - \frac{25}{24} g l + \frac{1}{4} g l = 0$$

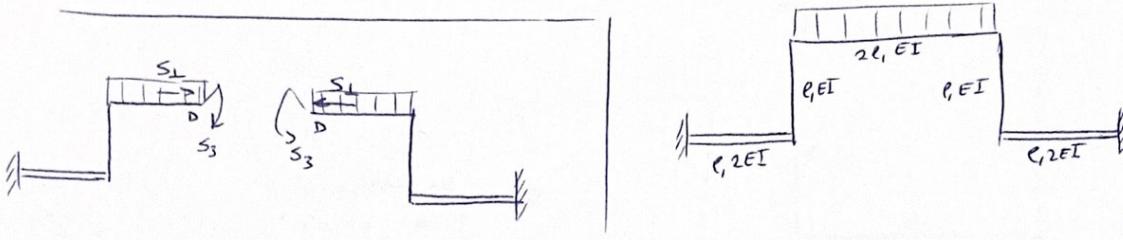
$$-\frac{16}{9} s_1 - \frac{19}{24} g l = 0$$

$$s_1 = -\frac{19 \cdot 9}{16 \cdot 24} g l = 1 \quad \underline{\underline{s_1 = -\frac{57}{128} g l}}$$

$$s_2 = -\frac{5}{3} \cdot \left(-\frac{57}{128} g l \right) - \frac{5}{8} g l$$

$$s_2 = \frac{95}{128} g l - \frac{80}{128} g l \Rightarrow \underline{\underline{s_2 = \frac{15}{128} g l}}$$

(10)



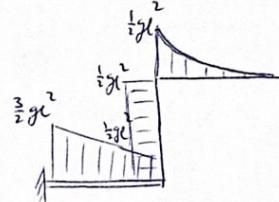
sim. konstrukcija, sim. opt. $\Rightarrow S_2 = 0$

1)

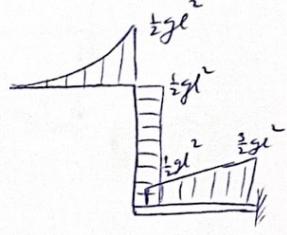
$$f_{D, \text{rec}}^{\text{har}} = \alpha_{11} S_1 + \alpha_{13} S_3 + \Delta_1^2 = 0$$

$$(2) f_{D, \text{rec}} = \alpha_{31} S_1 + \alpha_{33} S_3 + \Delta_3^2 = 0$$

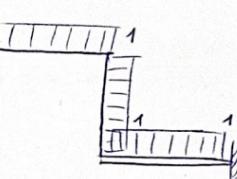
2)



3)



1



$$\alpha_{11} = \frac{1}{2EI} \left\{ e \cdot e \cdot e \right\} \cdot 2 + \frac{1}{EI} \left\{ \frac{1}{2} e \cdot e \cdot \frac{2}{3} e \right\} \cdot 2 = \frac{5}{3} \frac{e^3}{EI}$$

$$\alpha_{13} = \frac{1}{2EI} \left\{ e \cdot e \cdot 1 \right\} \cdot 2 + \frac{1}{EI} \left\{ \frac{1}{2} e \cdot e \cdot 1 \right\} \cdot 2 = 2 \frac{e^3}{EI}$$

$$\alpha_{33} = \frac{1}{2EI} \left\{ 1 \cdot e \cdot 1 \right\} \cdot 2 + \frac{1}{EI} \left\{ 1 \cdot e \cdot 1 \cdot 2 \right\} \cdot 2 = 5 \frac{e^3}{EI}$$

$$\Delta_1^2 = \frac{1}{2EI} \left\{ \frac{\frac{3}{2}gl^2 + \frac{1}{2}gl^2}{2} \cdot e \cdot e \right\} \cdot 2 + \frac{1}{EI} \left\{ \frac{1}{2}gl^2 \cdot e \cdot \frac{e}{2} \right\} \cdot 2 = \frac{3}{2} \frac{gl^4}{EI}$$

$$\Delta_3^2 = \frac{1}{2EI} \left\{ \frac{\frac{3}{2}gl^2 + \frac{1}{2}gl^2}{2} \cdot e \cdot 1 \right\} \cdot 2 + \frac{1}{EI} \left\{ \frac{1}{2}gl^2 \cdot e \cdot 1 + \frac{1}{3} \frac{1}{2}gl^2 \cdot e \cdot 1 \right\} \cdot 2 = \frac{7}{3} \frac{gl^3}{EI}$$

$$\frac{5}{3} \frac{e^3}{EI} S_1 + 2 \frac{e^3}{EI} S_3 + \frac{3}{2} \frac{gl^4}{EI} = 0 \quad | \cdot \frac{EI}{2e^2}$$

$$2 \frac{e^2}{EI} S_1 + 5 \frac{e^3}{EI} S_3 + \frac{7}{3} \frac{gl^3}{EI} = 0 \quad | \cdot \frac{EI}{e}$$

$$S_3 = -\frac{5}{6} S_1 e - \frac{3}{4} gl^2$$

$$2 S_1 e + 5 \left(-\frac{5}{6} S_1 e - \frac{3}{4} gl^2 \right) + \frac{7}{3} gl^2 = 0$$

$$2 S_1 e - \frac{25}{6} S_1 e - \frac{15}{4} gl^2 + \frac{7}{3} gl^2 = 0$$

$$-\frac{13}{6} S_1 e + \frac{17}{12} gl^2 = 0$$

$$S_1 = \frac{17 \cdot e}{12 \cdot 13} gl \Rightarrow S_1 = \frac{17}{26} gl$$

$$S_3 = -\frac{5}{6} \left(-\frac{17}{26} gl^2 \right) - \frac{3}{4} gl^2 = gl^2 \left(\frac{85}{156} - \frac{112}{156} \right) =$$

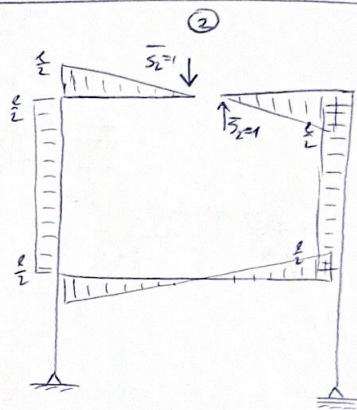
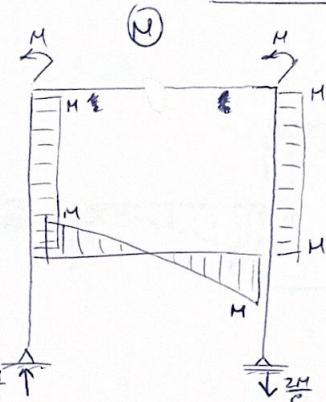
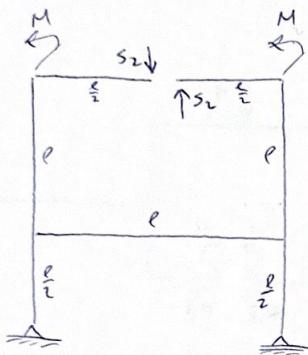
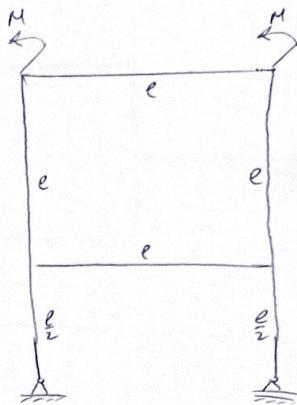
$$S_3 = -\frac{32}{156} gl^2 \Rightarrow S_3 = -\frac{8}{39} gl^2$$

(11)

$$EI = \text{const.}$$

sim. konstr.
 $(\alpha_{11}=0, \alpha_{22}=0)$, aufliegende opt. \Rightarrow
 $(\Delta_1=0, \Delta_2=0)$

$$\Rightarrow \alpha_{22} S_2 + \Delta_2 = 0$$



$$\alpha_{22} = ② \times ① = \frac{1}{EI} \left\{ \frac{1}{2} \frac{e}{2} \frac{e}{2} \frac{2}{3} \frac{e}{2} \cdot 4 + \frac{e}{2} e \frac{e}{2} \cdot 2 \right\} = \frac{e^3}{EI} \left(\frac{1}{6} + \frac{1}{2} \right) = \frac{2}{3} \frac{e^3}{EI}$$

$$\Delta_2 = ④ \times ① = \frac{1}{EI} \left\{ -Me \frac{e}{2} \cdot 2 - \frac{1}{2} M \frac{e}{2} \frac{2}{3} \frac{e}{2} \cdot 2 \right\} = \frac{Me^2}{EI} \left\{ -1 - \frac{1}{6} \right\} = -\frac{7}{6} \frac{Me^2}{EI}$$

$$\frac{2}{3} \frac{e^3}{EI} S_2 - \frac{7}{6} \frac{Me^2}{EI} = 0 \quad | \cdot \frac{6EI}{e^2}$$

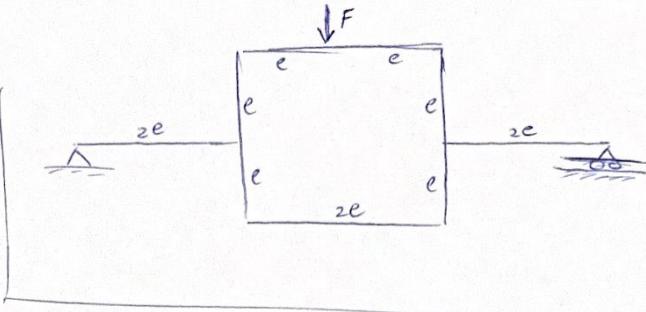
$$4 S_2 e - 7 M = 0$$

$$\boxed{S_2 = \frac{7}{4} \frac{M}{e}}$$

$$(12) \quad EI = \text{const}$$

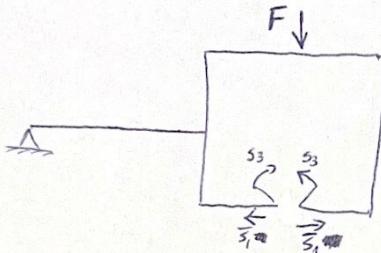
sm. konstruktions
 $(\alpha_{12} = 0, \alpha_{32} = 0)$, sm. opt.
 $(\Delta_2 = 0, \alpha_{13} = 0)$

$$\Rightarrow \underline{s_2 = 0}$$

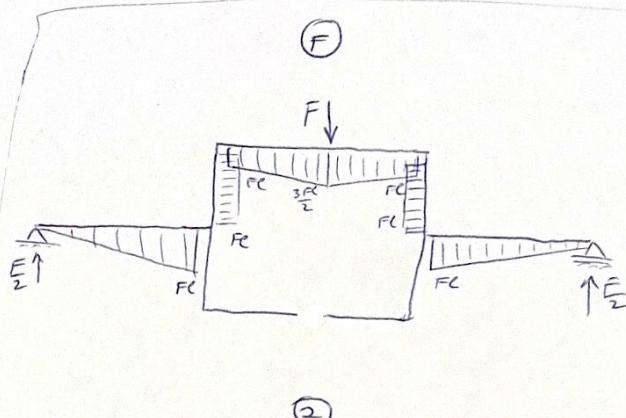


$$\alpha_{11} s_1 + \alpha_{31} s_3 + \Delta_1 = 0$$

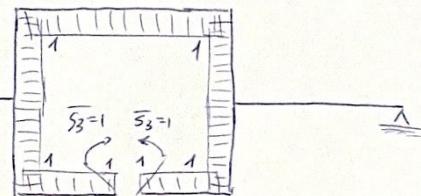
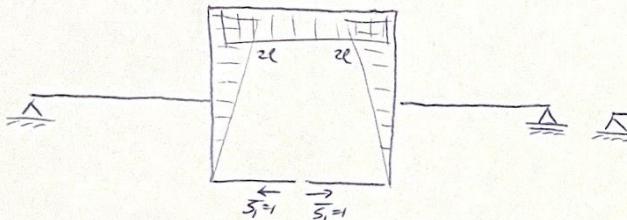
$$\alpha_{31} s_1 + \alpha_{33} s_3 + \Delta_3 = 0$$



①



②



$$\alpha_{11} = \frac{1}{EI} \left\{ \frac{1}{2} 2e \cdot 2e - \frac{2}{3} 2e \cdot 2 + 2e \cdot 2e \cdot 2e \right\} = \frac{e^3}{EI} \left\{ \frac{16}{3} + 8 \right\} = \frac{40}{3} \frac{e^3}{EI}$$

$$\alpha_{12} = \alpha_{21} = \frac{1}{EI} \left\{ 1 \cdot 2e \cdot e \cdot 2 + 1 \cdot 2e \cdot 2e \right\} = 8 \frac{e^2}{EI}$$

$$\alpha_{22} = \frac{1}{EI} \left\{ 1 \cdot e \cdot 1 \cdot 8 \right\} = 8 \frac{e}{EI}$$

$$\Delta_1 = \frac{1}{EI} \left\{ Fl \cdot e (e + \frac{1}{2}e) \cdot 2 + 2e \cdot e (Fl + \frac{1}{4}Fc) \cdot 2 \right\} = \frac{Fc^3}{EI} (3 + 5) = 8 \frac{Fc^3}{EI}$$

$$\Delta_2 = \frac{1}{EI} \left\{ Fl \cdot e \cdot 1 \cdot 2 + \frac{Fc + \frac{3}{2}Fc}{2} \cdot e \cdot 1 \cdot 2 \right\} = \frac{Fc^2}{EI} (2 + \frac{5}{2}) = \frac{9}{2} \frac{Fc^2}{EI}$$

$$\frac{40}{3} \frac{e^3}{EI} s_1 + 8 \frac{e^2}{EI} s_3 + 8 \frac{Fc^3}{EI} = 0 \quad | \cdot \frac{EI}{8e^2}$$

$$8 \frac{e^2}{EI} s_1 + 8 \frac{1}{EI} s_3 + \frac{9}{2} \frac{Fc^2}{EI} = 0 \quad | \cdot \frac{EI}{e}$$

$$\frac{5}{3} s_1 e + s_3 + Fl = 0 \quad | = \quad s_3 = -Fl - \frac{5}{3} s_1 e$$

$$8 s_1 e + 8(-Fl - \frac{5}{3} s_1 e) + \frac{9}{2} Fc = 0$$

$$-\frac{16}{3} s_1 e - \frac{7}{2} Fc = 0 \quad \Rightarrow \quad s_1 = -\frac{21}{32} \frac{Fc}{e}$$

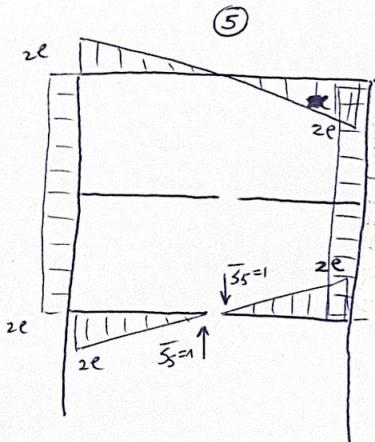
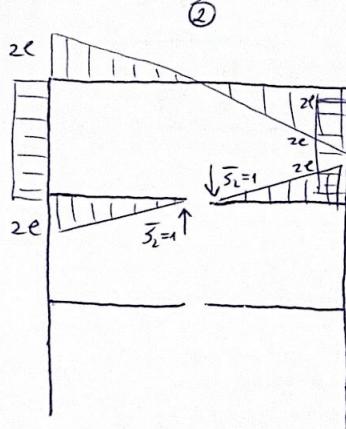
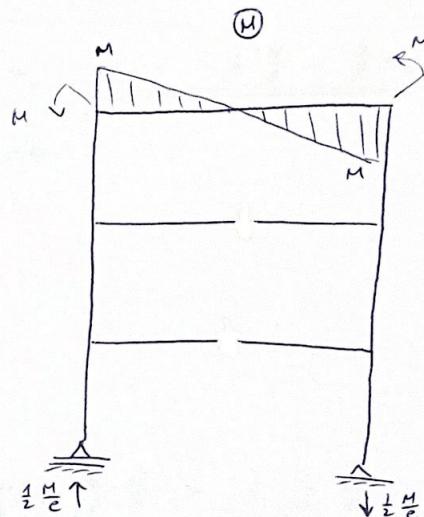
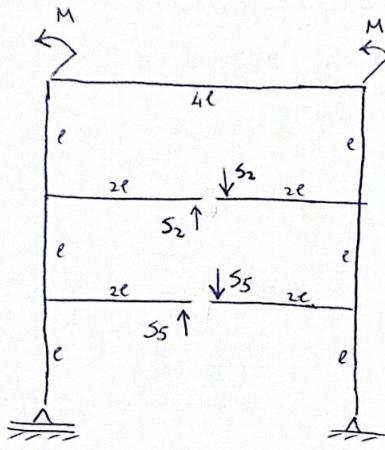
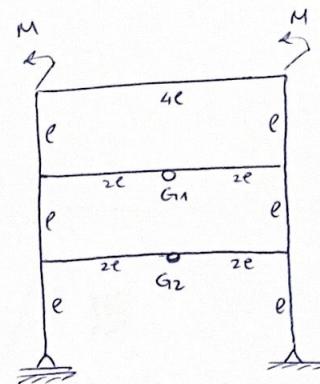
$$s_3 = -Fl + \frac{5}{3} \frac{21}{32} Fc \quad | = \quad s_3 = \frac{3}{32} Fc$$

$$(1) EI = \text{const.}$$

Stab. kons. , aufliegender opt. \Rightarrow
 \Rightarrow postope sawo transv. stabe

$$f_{G_1, \text{rel}}^{\text{vert}} = \alpha_{22} S_2 + \alpha_{25} S_5 + \Delta_2 = 0$$

$$f_{G_2, \text{rel}}^{\text{vert}} = \alpha_{52} S_2 + \alpha_{55} S_5 + \Delta_5 = 0$$



$$\alpha_{22} = \frac{1}{EI} \left\{ \frac{1}{2} 2e \cdot 2e \cdot \frac{2}{3} 2e \cdot 4 + 2e \cdot e \cdot 2e \cdot 2 \right\} = \frac{e^3}{EI} \left\{ \frac{32}{3} + 8 \right\} = \frac{56}{3} \frac{e^3}{EI}$$

$$\alpha_{25} = \frac{1}{EI} \left\{ \frac{1}{2} 2e \cdot 2e \cdot \frac{2}{3} 2e \cdot 2 + 2e \cdot e \cdot 2e \cdot 2 \right\} = \frac{e^3}{EI} \left\{ \frac{16}{3} + 8 \right\} = \frac{40}{3} \frac{e^3}{EI}$$

$$\alpha_{55} = \frac{1}{EI} \left\{ \frac{1}{2} 2e \cdot 2e \cdot \frac{2}{3} 2e \cdot 4 + 2e \cdot 2e \cdot 2e \cdot 2 \right\} = \frac{e^3}{EI} \left\{ \frac{32}{3} + 16 \right\} = \frac{80}{3} \frac{e^3}{EI}$$

$$\Delta_2 = \frac{1}{EI} \left\{ \frac{1}{2} M \cdot 2e - \frac{2}{3} 2e \cdot 2 \right\} = \frac{8}{3} \frac{Me^2}{EI}$$

$$\Delta_5 = \frac{1}{EI} \left\{ \frac{1}{2} M \cdot 2e - \frac{2}{3} 2e \cdot 2 \right\} = \frac{8}{3} \frac{Me^2}{EI}$$

$$\frac{5G}{3} \frac{e^3}{EI} S_2 + \frac{40}{3} \frac{e^3}{EI} S_5 + \frac{8}{3} \frac{Me^2}{EI} = 0 \quad / \cdot \frac{3EI}{8e^2}$$

$$\frac{40}{3} \frac{e^3}{EI} S_2 + \frac{80}{3} \frac{e^3}{EI} S_5 + \frac{8}{3} \frac{Me^2}{EI} = 0 \quad / \cdot \frac{3EI}{8e^2}$$

$$7S_2e + 5S_5e + M = 0 \Rightarrow S_5 = -\frac{1}{5} \frac{M}{e} - \frac{7}{5} S_2$$

$$5S_2e + 10 \left(-\frac{1}{5} \frac{M}{e} - \frac{7}{5} S_2 \right) e + M = 0$$

$$5S_2e - 2M - 14S_2e + M = 0$$

$$-9S_2e - M = 0$$

$$\boxed{S_2 = -\frac{1}{9} \frac{M}{e}}$$

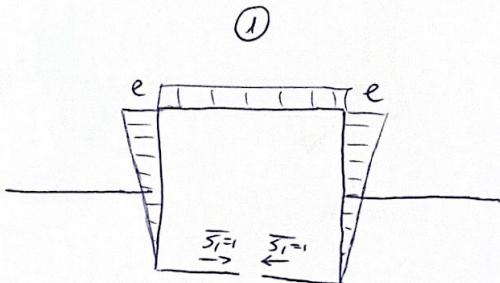
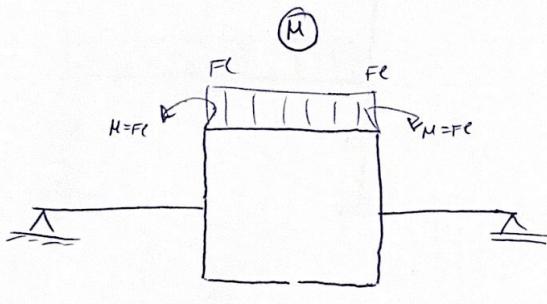
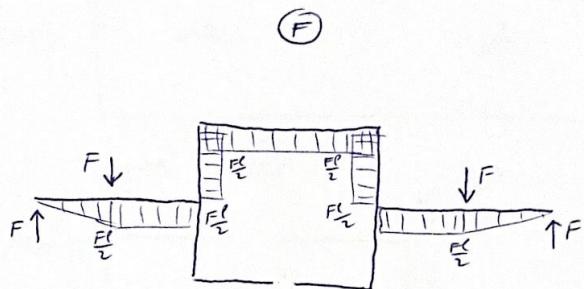
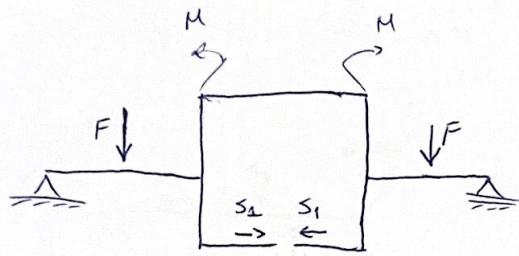
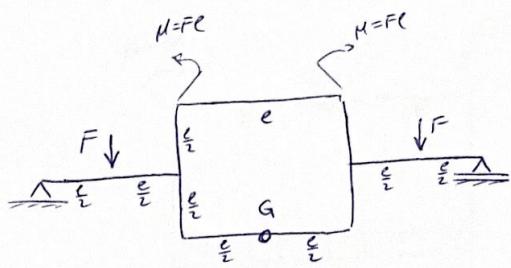
$$S_5 = -\frac{1}{5} \frac{M}{e} - \frac{7}{5} \left(-\frac{1}{9} \frac{M}{e} \right) = -\frac{1}{5} \frac{M}{e} + \frac{7}{45} \frac{M}{e} = -\frac{2}{45} \frac{M}{e}$$

$$\boxed{S_5 = -\frac{2}{45} \frac{M}{e}}$$

$$(14) \quad M = F\ell$$

$EI = \text{const.}$

sim. konserv., sim. opt. \Rightarrow
 $\Rightarrow S_2 = 0$



$$f_{G,\text{ree}}^{\text{hor}} = \alpha_{11} S_L + \Delta_1^F + \Delta_1^M = 0$$

$$\alpha_{11} = \frac{1}{EI} \left\{ \frac{1}{2} e \cdot e \cdot \frac{2}{3} e \cdot 2 + e \cdot e \cdot e \right\} = \frac{5}{3} \frac{e^3}{EI}$$

$$\Delta_1^F = \frac{1}{EI} \left\{ - \frac{F\ell}{2} \cdot \frac{\ell}{2} \left(\frac{\ell}{2} + \frac{e}{4} \right) \cdot 2 - \frac{F\ell}{2} \cdot e \cdot e \right\} = \frac{F\ell^3}{EI} \left(-\frac{3}{8} - \frac{1}{2} \right) = -\frac{7}{8} \frac{F\ell^3}{EI}$$

$$\Delta_1^M = \frac{1}{EI} (Fc \cdot e \cdot e) = \frac{Fc^3}{EI}$$

$$\frac{5}{3} \frac{e^3}{EI} S_L - \frac{7}{8} \frac{Fc^3}{EI} + \frac{Fc^3}{EI} = 0 \quad | \cdot 24 \frac{EI}{c^3}$$

$$40 S_L + 3 F = 0$$

$$\boxed{S_L = -\frac{3}{40} F}$$

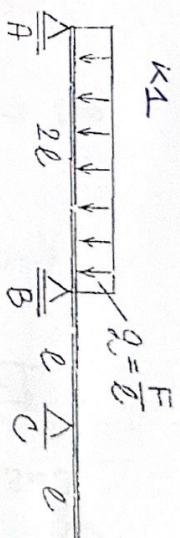
ОСНОВА ОТПОРНОСТИ КОНСТРУКЦИЈА

Пријемни испит из
јунски испитни рок 2008.

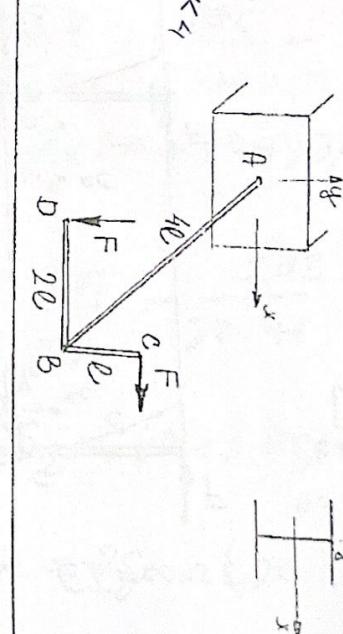
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κ_1

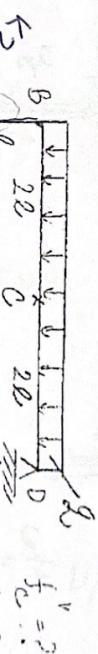
∠ опртја



2.



3.



1. Носач ABCD константног попречног пресека отпремен је концентрисаном снажом F и континуалним отпремњем $q=F/l$. Највећи дужарни момент монтирана савијања.
2. Носач ABCD просторно је отпремен према снажи. Користећи Хинтезу максималних тангенцијалних напона одредити највећи резултујући напон у конструкцији ако је попречни пресек:
- Пуни круг $\mathcal{O}_d = 9 \text{ cm}$,
 - Стандардни профил I 26.
- I група: $F=5 \text{ kN}$, $l=40 \text{ cm}$
II група: $F=7 \text{ kN}$, $l=30 \text{ cm}$

3. Равански статички одређени носач ABCD константног попречног пресека отпремен је према склопу. Одредити хоризонтално покретање пресека K и вертикално покретање пресека C.

4. Равански носач са зглобом G отпремен је континуалним отпремњем q и моментом M .
- Редовни носач и највећи дужарни момент монтирана савијања.
 - Одредити максималну вредност момента M ако је дозвољени напон $\sigma_{\text{doz}}=8 \text{ kN/cm}^2$, а попречни пресек стандардни профил I 14,
- I група: I 14,
II група: I 16.

Напомене:

- Испит траје три сата.
- Резултати не бићи објављени до петка 4. јула у 15 сата.
- Не користити сиске, једије за напака, мобилне телефоне!

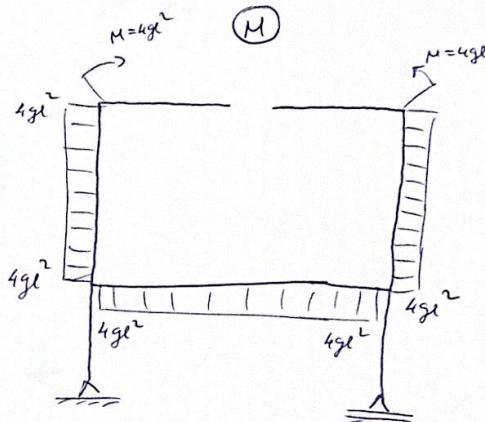
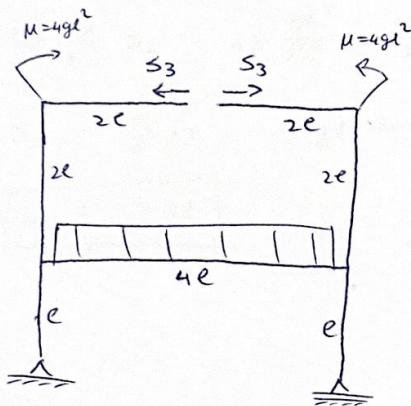
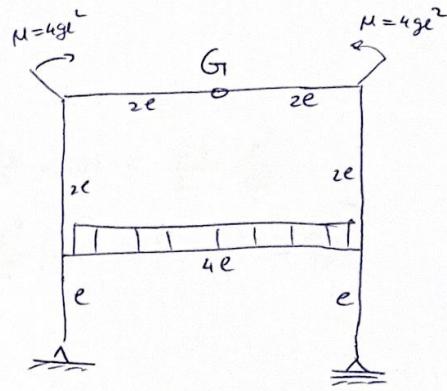
- у Београду, 01.07.2008. год.
ČASOVNI POKLJUNO
Profesor NENAD
064/155-72-42

jun 08

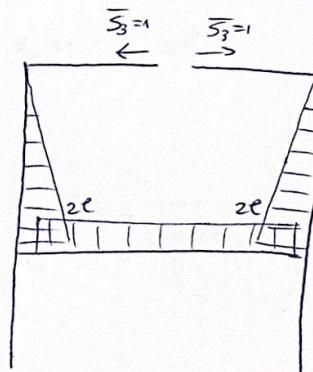
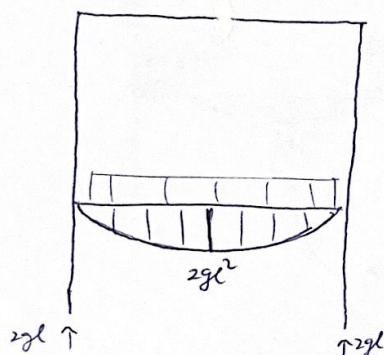
$$④ M = 4gl^2, EI = \text{const.}$$

odrediti max. vrijednost momenta M ,
ako je $\sigma_{\text{dop}} = 8 \frac{\text{kN}}{\text{cm}^2}$, $I/4$

sim konst, str. opt. $\Rightarrow S_2 = 0$



⑤



$$M = 2gl \cdot z - gz \cdot \frac{z}{2} = -\frac{1}{2}gz^2 + 2gl \cdot z$$

$$z=0 \Rightarrow M=0$$

$$z=2l \Rightarrow M = -\frac{1}{2}4gl^2 + 2gl \cdot 2l = 2gl^2$$

$$z=4l \Rightarrow M=0$$

$$f_{G, \text{rec}}^{\text{har}} = \alpha_{11} S_1 + \Delta_1^H + \Delta_1^S = 0$$

$$\alpha_{11} = \frac{1}{EI} \left\{ \frac{1}{2} 2e \cdot 2e \cdot \frac{2}{3} 2e \cdot 2 + 2e \cdot 4e \cdot 2e \right\} = \frac{e^3}{EI} \left(\frac{16}{3} + 16 \right) = \frac{64}{3} \frac{e^3}{EI}$$

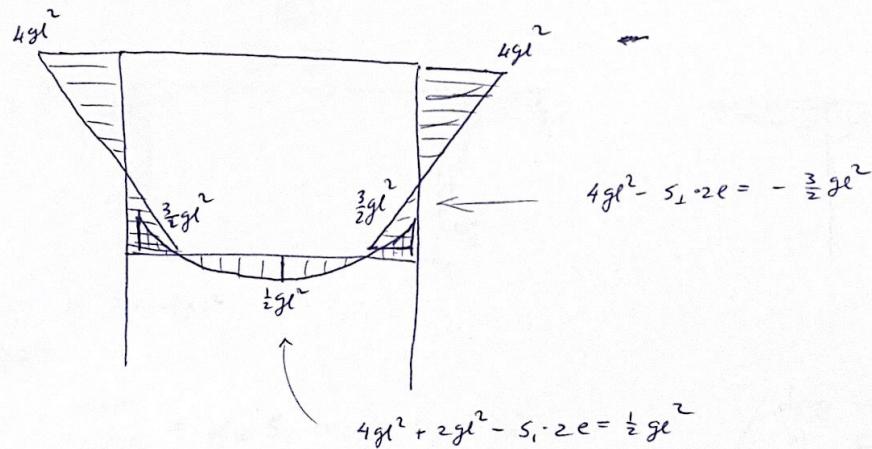
$$\Delta_1^H = \frac{1}{EI} \left\{ -4ge^2 \cdot 2e \cdot e \cdot 2 - 4ge^2 \cdot 4e \cdot 2e \right\} = \frac{ge^4}{EI} (-16 - 32) = -48 \frac{ge^4}{EI}$$

$$\Delta_1^S = \frac{1}{EI} \left\{ -2 \cdot \frac{2}{3} \cdot 2ge^2 \cdot 2e \cdot 2e \right\} = -\frac{32}{3} \frac{ge^4}{EI}$$

$$\frac{64}{3} \frac{ge^3}{EI} S_1 - 48 \frac{ge^4}{EI} - \frac{32}{3} \frac{ge^4}{EI} = 0 \quad | \cdot \frac{3}{64} \frac{EI}{e^3}$$

$$S_1 - \frac{9}{4} ge - \frac{1}{2} ge = 0$$

$$\boxed{S_1 = \frac{11}{4} ge}$$



$$\sigma_{\max} = \frac{4ge^2}{w_x} = \frac{M}{w_x} \leq \sigma_{\text{dop}}$$

$$M \leq \sigma_{\text{dop}} \cdot w_x = 8 \frac{kN}{cm^2} \cdot 81,9 \text{ cm}^3 = 655,2 \text{ kNm} \Rightarrow \boxed{M_{\max} = 655 \text{ kNm}}$$

$$w_x = 81,9 \text{ cm}^3 - \text{zu } I14$$

Задатак 1.

Писани испит из ООК

-Октобар (диплумски рок) 2011.-

1. Континуални гредни посач константне кривоти оптерећен је према скеми.

- Пријеком Методе растављања решити посач и најкрати статичке дужине.

- Преко преносила момента у пресеку изнад осовина В извиши димензионисане ногеши, ако је пресек направљен од стандарданог I-профилда JUS-C-B3-131. Потребни бројни подаци: $q=4kN/cm$; $l=60cm$.

2. Задати статички неодређени радијусни посач оптерећен је према скеми.

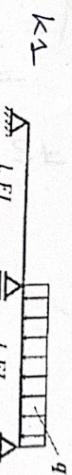
- Одредити статички непознате величине и најкрати дужине момената – Вертикалним поступком, користећи особину симетрије.

3. Просторни посач константног кружног попречног пресека оптерећен је према скеми.

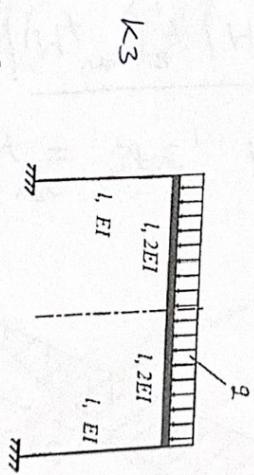
- Најкрати статичке појатражве (она сваке сице појединачно).

- Еквивалентни напон у пресеку A срачунати применом Хинштегејеве формуле напона симултана, па димензионисани посач ($\delta d = ?$) уколико је дозвољени напон $\sigma_{de} = 10kN/cm^2$ при чулу је $F=1kN$ и $l=60cm$.

Задатак 2.

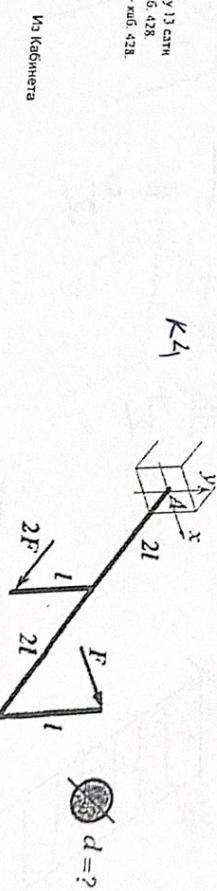


Задатак 3.



- Напомена:
Испит траје три сата
Дозволено је саопштавајући материјала – не заборав!
Резултати ће бити објављени најкасније до понедељка 14.11.2011. у 13 часова
Увод у испитне радове: понедељак 14.11.2011. год. у 13 часова – изб. 428
Уведен део испита објавље је уторак 15.11.2011. год. у 13 часова – изб. 428

У Београду, 13.11.2011. год.

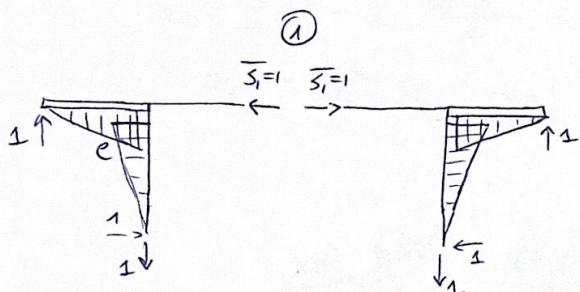
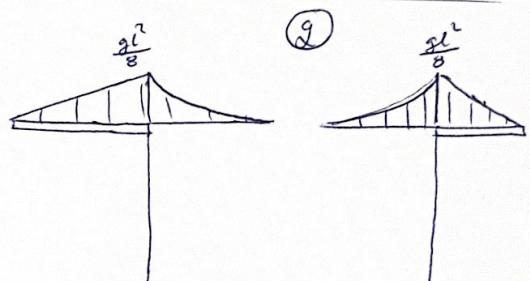
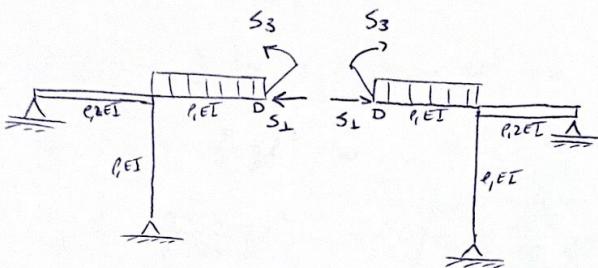
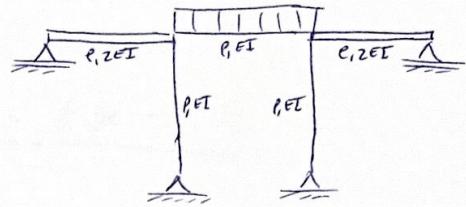


Испитни лист

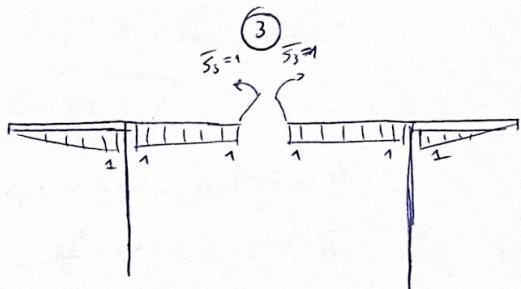
otobar II

② naertah zGini diagram
momenta saijauja

$$\text{sim. kausi, sim. opd.} \Rightarrow S_2 = 0$$



$$M_f = -gz \cdot \frac{z}{2} = -\frac{1}{2}gz^2$$



$$(1) f_{D, \text{rec}}^{\text{hor}} = \alpha_{11} S_1 + \alpha_{13} S_3 + \Delta_1^2 = 0$$

$$(2) \varphi_{D, \text{rec}} = \alpha_{31} S_1 + \alpha_{33} S_3 + \Delta_3^2 = 0$$

drugi učin G: G:0:
 (1) $f_{D, e}^{\text{hor}} = -f_{D, d}^{\text{hor}}$
 (2) $\varphi_{D, e} = -\varphi_{D, d}$
 pa G_i oduz posvetlji koo posljuge dijagrome (2) (2) (1) (1) (3) (3)

$$\alpha_{11} = \frac{1}{2EI} \left\{ \frac{1}{2} \ell \cdot \ell \cdot \frac{2}{3} \ell \right\} \cdot 2 + \frac{1}{EI} \left\{ \frac{1}{2} \ell \cdot \ell \cdot \frac{2}{3} \ell \right\} \cdot 2 = \frac{\ell^3}{EI} \left(\frac{1}{3} + \frac{2}{3} \right) = \frac{\ell^3}{EI}$$

$$\alpha_{13} = \frac{1}{2EI} \left\{ \frac{1}{2} \ell \cdot \ell \cdot \frac{2}{3} \cdot 1 \right\} \cdot 2 = \frac{1}{3} \frac{\ell^2}{EI}$$

$$\alpha_{33} = \frac{1}{2EI} \left\{ \frac{1}{2} \cdot 1 \cdot \ell \cdot \frac{2}{3} \cdot 1 \right\} \cdot 2 + \frac{1}{EI} \left\{ 1 \cdot \frac{\ell}{2} \cdot 1 \right\} \cdot 2 = \frac{\ell}{EI} \left(\frac{1}{3} + 1 \right) = \frac{4}{3} \frac{\ell}{EI}$$

$$\Delta_1^2 = \frac{1}{2EI} \left\{ -\frac{1}{2} \frac{gl^2}{8} \cdot \ell \cdot \frac{2}{3} \ell \right\} \cdot 2 = -\frac{1}{24} \frac{gl^4}{EI}$$

$$\Delta_3^2 = \frac{1}{2EI} \left\{ -\frac{1}{2} \frac{gl^2}{8} \cdot \ell \cdot \frac{2}{3} \ell \right\} \cdot 2 + \frac{1}{EI} \left\{ \frac{1}{3} \frac{gl^2}{8} \cdot \frac{1}{2} \cdot 1 \right\} \cdot 2 = \frac{gl^3}{EI} \left(-\frac{1}{24} - \frac{1}{24} \right) = -\frac{1}{12} \frac{gl^3}{EI}$$

$$(1) \quad \frac{e^3}{EI} s_1 + \frac{1}{3} \frac{e^2}{EI} s_3 - \frac{1}{24} \frac{ge^4}{EI} = 0 \quad | \cdot \frac{EI}{e^3}$$

$$(2) \quad \frac{1}{3} \frac{e^2}{EI} s_1 + \frac{4}{3} \frac{e}{EI} s_3 - \frac{1}{12} \frac{ge^3}{EI} = 0 \quad | \cdot 12 \frac{EI}{e}$$

$$(1) \quad s_1 + \frac{1}{3} \frac{s_3}{e} - \frac{1}{24} gl = 0 \Rightarrow s_1 = \frac{1}{24} gl - \frac{1}{3} \frac{s_3}{e}$$

$$(2) \quad 4s_1 e + 16s_3 - gl^2 = 0$$

$$4\left(\frac{1}{24}gl - \frac{1}{3}\frac{s_3}{e}\right)e + 16s_3 - gl^2 = 0$$

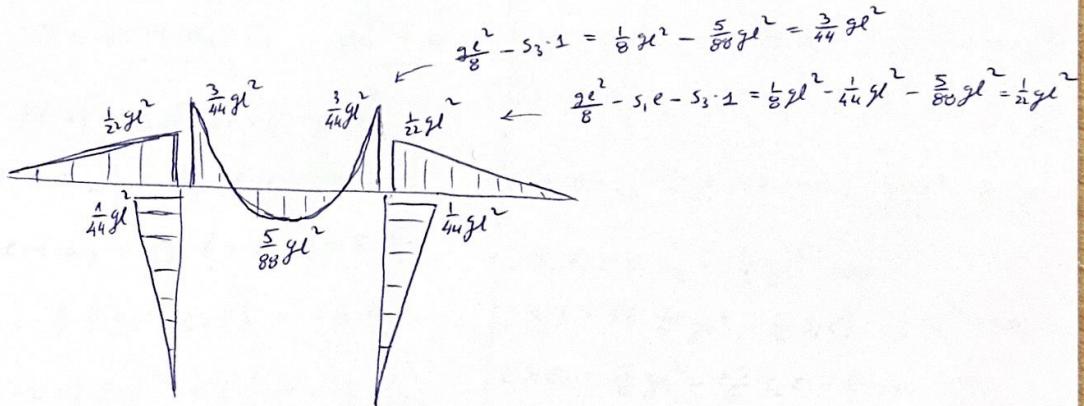
$$\frac{1}{6}gl^2 - \frac{4}{3}s_3 + 16s_3 - gl^2 = 0$$

$$\frac{44}{3}s_3 - \frac{5}{6}gl^2 = 0$$

$$s_3 = \frac{5 \cdot 3}{6 \cdot 44} gl^2 \Rightarrow \boxed{s_3 = \frac{5}{88} gl^2}$$

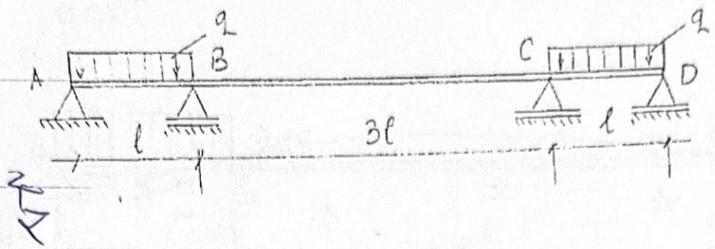
$$(1) \quad s_1 = \frac{1}{24}gl - \frac{1}{3} \frac{\frac{5}{88}gl^2}{e} = gl\left(\frac{1}{24} - \frac{5}{264}\right) = gl\left(\frac{11}{264} - \frac{5}{264}\right) =$$

$$\Rightarrow s_1 = \frac{6}{264} gl \Rightarrow \boxed{s_1 = \frac{1}{44} gl}$$



II ГРУПА

1.



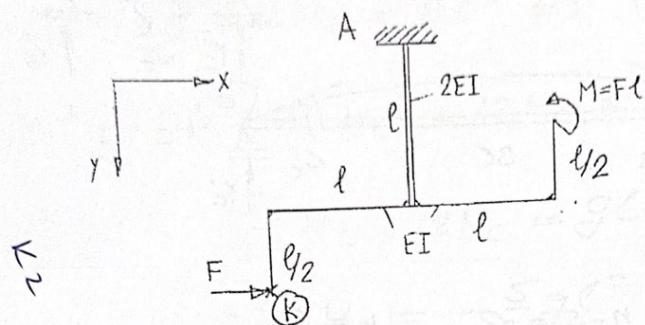
$$\sigma_{\max} = ?$$

$$q = 5 \text{ [kN/m]}$$

$$l = 200 \text{ [cm]}$$

$\frac{T \text{ DIN 1024}}{T 120}$

2.

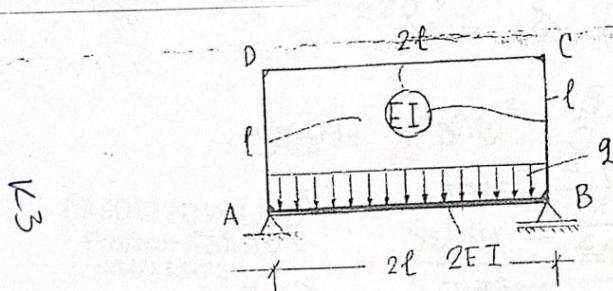


$$f_k^y = ?$$

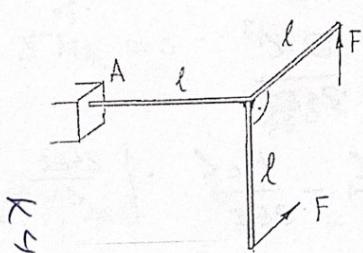
$$f_k^x = ?$$

$$\varphi_k = ?$$

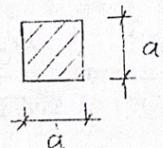
3.



4.

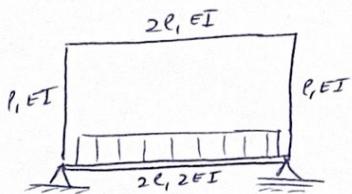


$$\left. \begin{array}{l} a) \quad \phi d = 5 \text{ [cm]} \\ b) \quad \phi d = 5 \text{ [cm]} \end{array} \right\} \begin{array}{l} F = 2 \text{ [kN]} \\ l = 50 \text{ [cm]} \end{array}$$

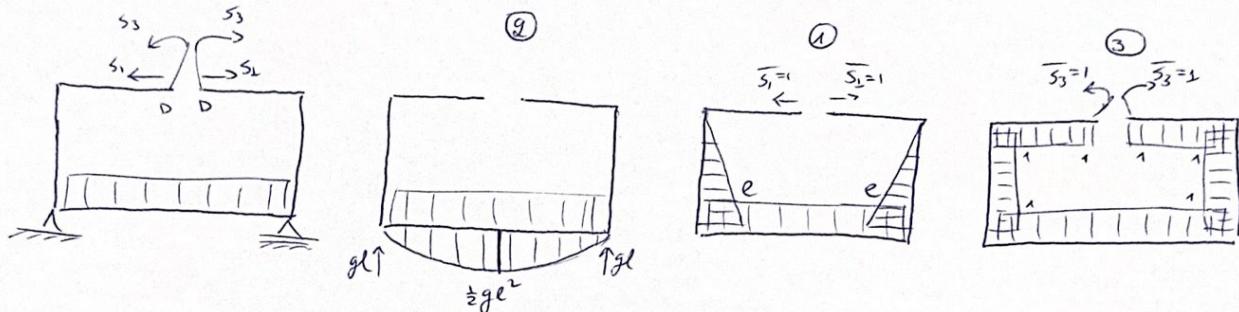


nepoznat rok

- ③ nacrtati zginu dijagram
wspomneta sa vijajući



$$\text{sim. kov.}, \text{ sim. opt.} \Rightarrow S_2 = 0$$



$$\mu_f = gl^2 - gz \cdot \frac{z}{2} = -\frac{1}{2}gz^2 + gl \cdot z; \begin{matrix} z=0 \\ z=l \\ z=2e \\ z=2e \end{matrix} \Rightarrow \begin{matrix} \mu=0 \\ \mu=\frac{1}{2}gl^2 \\ \mu=0 \\ \mu=0 \end{matrix}$$

$$(1) f_{D,\text{rec}}^{hor} = \alpha_{11} S_1 + \alpha_{13} S_3 + \Delta_1^2 = 0$$

$$(2) \varphi_{D,\text{rec}} = \alpha_{31} S_1 + \alpha_{33} S_3 + \Delta_3^2 = 0$$

$$\alpha_{11} = \frac{1}{EI} \left\{ \frac{1}{2} e \cdot e \cdot \frac{2}{3} e \cdot 2 \right\} + \frac{1}{2EI} \left\{ e \cdot 2e \cdot e \right\} = \frac{5}{3} \frac{e^3}{EI}$$

$$\alpha_{13} = \frac{1}{EI} \left\{ \frac{1}{2} e \cdot e \cdot 1 \cdot 2 \right\} + \frac{1}{2EI} \left\{ e \cdot 2e \cdot 1 \right\} = 2 \frac{e^2}{EI}$$

$$\alpha_{33} = \frac{1}{EI} \left\{ 1 \cdot e \cdot 1 \cdot 4 \right\} + \frac{1}{2EI} \left\{ 1 \cdot 2e \cdot 1 \right\} = 5 \frac{e}{EI}$$

$$\Delta_1^2 = \frac{1}{2EI} \left\{ -2 \cdot \frac{2}{3} \frac{1}{2} gl^2 \cdot e \cdot e \right\} = -\frac{1}{3} \frac{gl^4}{EI}$$

$$\Delta_3^2 = \frac{1}{2EI} \left\{ -2 \cdot \frac{2}{3} \frac{1}{2} gl^2 \cdot e \cdot 1 \right\} = -\frac{1}{3} \frac{gl^3}{EI}$$

$$(1) = 1 \frac{5}{3} \frac{e^3}{EI} S_1 + 2 \frac{e^2}{EI} S_3 + \frac{1}{3} \frac{gl^4}{EI} = 0 \quad | \cdot \frac{EI}{2e^2}$$

$$(2) = 1 2 \frac{e^2}{EI} S_1 + 5 \frac{e}{EI} S_3 - \frac{1}{3} \frac{gl^3}{EI} = 0 \quad | \cdot \frac{EI}{e}$$

$$\frac{5}{6} S_1 e + S_3 - \frac{1}{6} gl^2 = 0 \Rightarrow S_3 = \frac{1}{6} gl^2 - \frac{5}{6} S_1 e$$

$$2 S_1 e + 5 S_3 - \frac{1}{3} gl^2 = 0$$

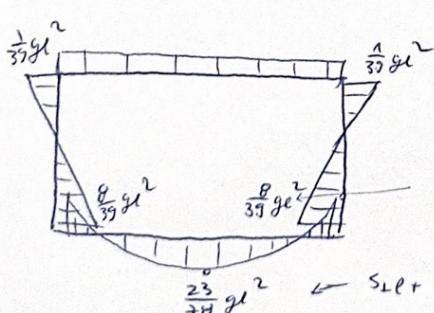
$$2 S_1 e + 5 \left(\frac{1}{6} gl^2 - \frac{5}{6} S_1 e \right) - \frac{1}{3} gl^2 = 0$$

$$2 S_1 e + \frac{5}{6} gl^2 - \frac{25}{6} S_1 e - \frac{1}{3} gl^2 = 0$$

$$-\frac{13}{6} S_1 e + \frac{1}{2} gl^2 = 0 \Rightarrow S_1 = \frac{3}{13} gl$$

$$S_3 = \frac{1}{6} gl^2 - \frac{5}{6} \frac{3}{13} gl^2 = \frac{1}{6} gl^2 - \frac{5}{26} gl^2 =$$

$$S_3 = \frac{26}{156} gl^2 - \frac{30}{156} gl^2 \Rightarrow S_3 = -\frac{1}{39} gl^2$$



$$S_1 e + S_3 e = \frac{3}{13} gl^2 - \frac{1}{39} gl^2 = \frac{8}{39} gl^2$$

$$S_1 e + S_3 e - \frac{1}{2} gl^2 = \frac{3}{13} gl^2 - \frac{1}{39} gl^2 - \frac{1}{2} gl^2 = \frac{23}{78} gl^2$$